

Partially Prism-Gridded FDTD Analysis for Layered Structures of Transversely Curved Boundary

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Abstract

A partially prism-gridded FDTD analysis is presented to deal with layered structures with curved boundary in transverse directions. It is applied to calculate the scattering parameters of vias in multilayer packaging. The good agreement of the results with those by other methods verifies the accuracy of this analysis.

Introduction

The finite-difference time-domain (FDTD) method has found a lot of applications in dealing with various electromagnetic problems. Originally developed for structures which can fit well into Cartesian coordinates [1], it suffers from significant degradation in accuracy for structures with curved boundary due to the staircasing approximation. Several attempts have been tried to alleviate the drawback by exploiting conformity to the solution region either globally or locally. Among them a very versatile and accurate one is a recently proposed hybrid method which employs the conventional FDTD method for most of the regular region and introduces the tetrahedral edge-based finite element scheme to model the re-

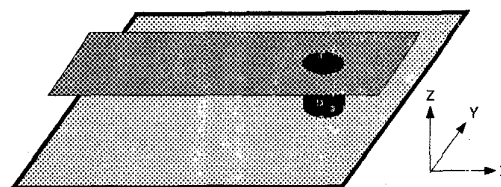


Fig.1 Geometry of microstrip with via hole ground ($\epsilon_r = 2.32$ and dielectric height = 0.8mm)

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2D

gion near the curved surfaces [2],[3]. Numerical results of simulation validate that the hybrid method has the advantages of accuracy, flexibility, and computational efficiency.

For most microwave devices, such as planar circuits, waveguides with step transitions, and packaging interconnections, the structures can be longitudinally divided into several building layers inside which the material and conductors can be of arbitrary shape in the transverse directions. The mesh need only call for triangular cells near the curved boundary in x-y directions while remaining rectangular grid in the z-direction. Hence, the generation of tetrahedral cells and the relatively time-consuming matrix solution of three-dimensional finite element method can be greatly simplified. A novel hybrid method is thus proposed in this paper which employs two-dimensional hybrid FD-FEM-TD method in each layer [2] and finite difference method to link the relationship of fields between layers

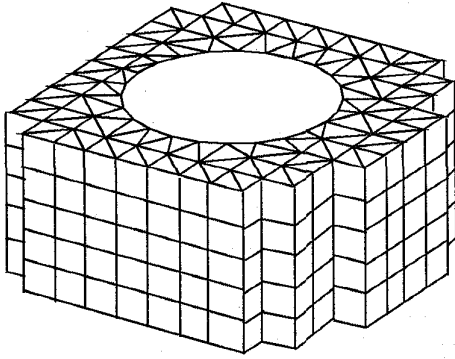


Fig.2 The prism cells around via hole

along the z direction.

Weak-form formulations in FEM region

Fig.1 shows an illustrative example of microstrip line with cylindrical grounded via. Using a uniform grid in the z -direction, the mesh division in the x, y plane consists of triangular elements near the via and regular FDTD grid elsewhere as shown in Fig.2. Consequently, there are prism cells formed by the triangular elements in the transverse plane together with the uniform grid in the z direction. Fig.3 shows the field discretization in a prism cell where the transverse components \vec{E}_ρ are located in integer z coordinate layer while the longitudinal components E_z are situated in half integer z coordinate layer.

Starting from the source-free Maxwell's two curl equations in a linear isotropic region, the vector wave equation can be obtained as

$$\nabla \times \left(\frac{1}{\mu} \nabla \times \vec{E} \right) + \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0 \quad (1)$$

Based on the variational reaction theory [4], (1) can be cast into the weak form by considering the inner product between (1) and an ar-

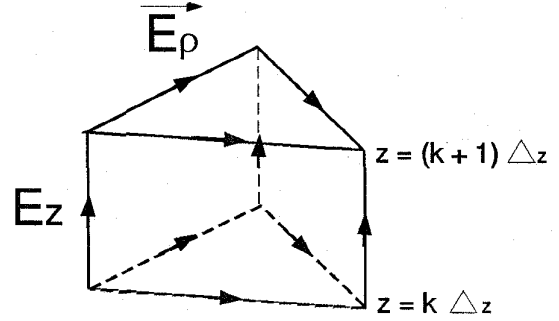


Fig.3 The prism element

bitrary testing field \vec{E}^a . Choosing transversely polarized field \vec{E}_ρ^a in the $z = k\Delta_z$ plane as the testing field and performing some simplifications, one may obtain

$$\begin{aligned} & \int_A \left\{ \frac{1}{\mu} \nabla_\rho \times \vec{E}_\rho^a \cdot \nabla_\rho \times \vec{E}_\rho + \epsilon \vec{E}_\rho^a \cdot \frac{\partial^2 \vec{E}_\rho}{\partial t^2} \right. \\ & \left. + \vec{E}_\rho^a \cdot \left[\frac{\partial}{\partial z} \left(\frac{1}{\mu} \nabla_\rho E_z \right) - \frac{\partial}{\partial z} \left(\frac{1}{\mu} \frac{\partial \vec{E}_\rho}{\partial z} \right) \right] \right\} dS \\ & = 0 \end{aligned} \quad (2a)$$

Here, ∇_ρ denotes the transverse del operator, \vec{E}_ρ the transverse components of the electric field and E_z the z -component. Similarly, in the $z = (k + \frac{1}{2})\Delta_z$ plane, one obtain

$$\begin{aligned} & \int_A \frac{1}{\mu} \nabla_\rho E_z^a \cdot \nabla_\rho E_z + \epsilon E_z^a \cdot \frac{\partial^2 E_z}{\partial t^2} \\ & - \frac{1}{\mu} \nabla_\rho E_z^a \cdot \frac{\partial \vec{E}_\rho}{\partial z} dS = 0 \end{aligned} \quad (2b)$$

for arbitrary testing field \vec{E}_z^a .

The weak form (2) can be discretized into a matrix form by choosing suitable basis functions. Here, the cross-sectional area A is subdivided into small triangular elements. The transverse components \vec{E}_ρ is expanded by edge-based Whitney function, i.e.,

$$\vec{E}_\rho|_{z=k\Delta_z} = \sum_i \vec{W}_i e_{\rho i} = \{\vec{W}\}^T \{e_\rho\}_k \quad (3)$$

while the longitudinal components E_z by node-based interpolation function, i.e.,

$$E_z|_{z=(k+\frac{1}{2})\Delta_z} = \sum_i \lambda_i e_{zi} = \{\lambda\}^T \{e_z\}_{k+\frac{1}{2}} \quad (4)$$

The testing fields \vec{E}_ρ^a and E_z^a are expanded by the two corresponding basis functions. Taking integration with respect to the basis functions and applying the Ritz procedure, (2) can be reduced to two systems of coupled differential equations for transverse and longitudinal components.

Based on the Crank-Nicolson scheme, we apply central finite difference method with respect to z and t variables and in addition take timing average for the first term in (2) [3]. The final time marching equation in the FEM region is

$$\begin{aligned} [G_{\rho\rho}^+]\{e_\rho\}_k^{n+1} &= 2[G_{\rho\rho}^-]\{e_\rho\}_k^n - [G_{\rho\rho}^+]\{e_\rho\}_k^{n-1} \\ &\quad - [C_{\rho z}](\{e_z\}_{k+\frac{1}{2}}^n - \{e_z\}_{k-\frac{1}{2}}^n) \\ &\quad + [D_{\rho\rho}](\{e_\rho\}_{k+1}^n - 2\{e_\rho\}_k^n \\ &\quad + \{e_\rho\}_{k-1}^n) \end{aligned} \quad (5a)$$

and

$$\begin{aligned} [G_{zz}^+]\{e_z\}_{k+\frac{1}{2}}^{n+1} &= 2[G_{zz}^-]\{e_z\}_{k+\frac{1}{2}}^n - [G_{zz}^+]\{e_z\}_{k+\frac{1}{2}}^{n-1} \\ &\quad + [C_{\rho z}]^T(\{e_\rho\}_{k+1}^n - \{e_\rho\}_k^n) \end{aligned} \quad (5b)$$

in which

$$\begin{aligned} [G_{\rho\rho}^\pm] &= \int_A \epsilon_r \{\vec{W}\} \{\vec{W}\}^T dS \\ &\quad \pm \frac{\kappa^2}{4} \int_A \frac{1}{\mu_r} \{\nabla_\rho \times \vec{W}\} \{\nabla_\rho \times \vec{W}\}^T dS \\ [C_{\rho z}] &= \kappa^2 \int_A \frac{1}{\mu_r} \{\vec{W}\} \{\nabla_\rho \lambda\}^T dS \\ [D_{\rho\rho}] &= \kappa^2 \int_A \frac{1}{\mu_r} \{\vec{W}\} \{\vec{W}\}^T dS \\ [G_{zz}^\pm] &= \int_A \epsilon_r \{\lambda\} \{\lambda\}^T dS \\ &\quad \pm \frac{\kappa^2}{4} \int_A \frac{1}{\mu_r} \{\nabla_\rho \lambda\} \{\nabla_\rho \lambda\}^T dS \end{aligned}$$

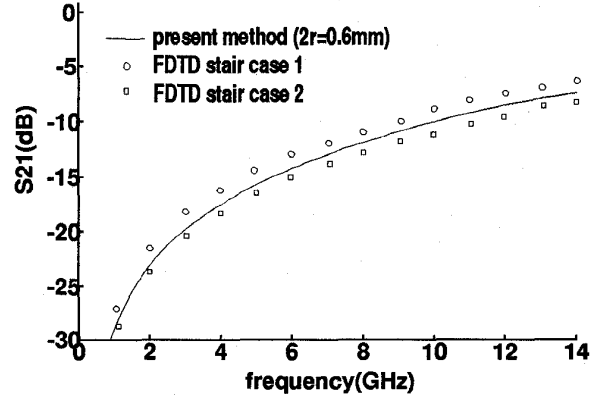


Fig.4 Comparison of the calculated $|S21|$ with staircasing FDTD method

Here, $\kappa = \frac{\Delta_t}{\sqrt{\mu_0 \epsilon_0} \Delta}$ is stability factor, the superscript of $\{e_\rho\}$ and $\{e_z\}$ stands for the time step and the subscript denotes the step in z coordinate. The time marching scheme is the same as that described in [3], except that the electric field of unregular regions is computed by (5) layer by layer at each time step.

Numerical results

A. Grounded via

This hybrid method has been employed to characterize the microstrip with cylindrical grounded via shown in Fig.1. Fig.4 compares the calculated scattering parameters with those by two staircasing FDTD analyses [5], for which model 1 approximates the via using the inner bounded staircase while model 2 the outer bounded staircase. As expected, the results by the present hybrid method lie somewhere in between.

Fig.5 compares the calculated results with those by mode matching method [6]. Good agreement can be noticed.

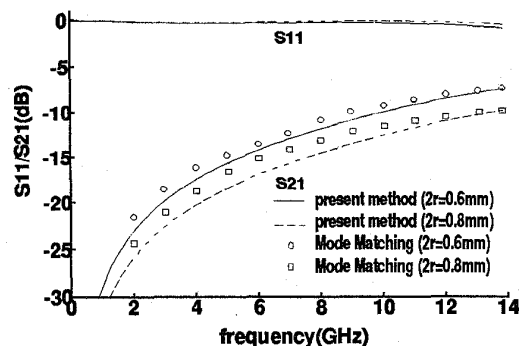


Fig.5 Comparison of the calculated $|S_{21}|$ with mode matching method

B. Through hole via

The approach is also applied to deal with the through hole vias in multilayer packaging structures as shown in the inset of Fig.6. The region near the rod is modeled by prism-gridded FEM. Fig.6 compares the calculated results with those by measured [7]. Good agreement verifies that the present method is capable of characterizing objects with curve boundary.

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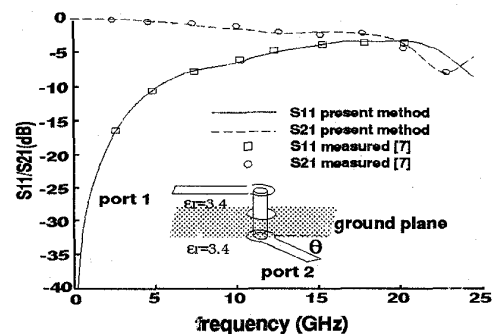


Fig.6 Comparison of the calculated $|S_{11}|$ and $|S_{21}|$ with measured results [7] (Each width of microstrips is 3.3mm and the diameter of the rod and the clearance hole is 1.5mm and 3.9mm respectively. $\theta = 0^\circ$)

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