



## A VELOCITY-OVERSHOOT CAPACITANCE MODEL FOR 0.1 $\mu\text{m}$ MOS TRANSISTORS

J. B. KUO\*, Y. W. CHANG and C. S. LAI

Rm 338, Department of Electrical Engineering, National Taiwan University, Roosevelt Rd, Sec. 4, #1,  
Taipei, Taiwan 106-17

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**Abstract**—This article discusses an analytical velocity-overshoot capacitance model for a 0.1  $\mu\text{m}$  MOS transistor. As verified by 2D simulation results, compared to the conventional model the analytical capacitance model considering velocity overshoot shows a smaller  $C_{\text{SG}}$  and  $C_{\text{DG}}$  value, because in velocity overshoot a smaller amount of electrons exist in the channel region. Compared to the  $C_{\text{SG}}$  case, the larger decrease in  $C_{\text{DG}}$  when considering velocity overshoot at high  $V_{\text{D}}$  is the result of higher electron velocity in the post-saturation region. Copyright © 1996 Elsevier Science Ltd

### 1. INTRODUCTION

For decades the evolution of MOS devices has already been consistently continued. Sub-0.1  $\mu\text{m}$  MOS devices for next generation VLSI have been reported[1]. Since the supply voltage can't be scaled down sufficiently for deep submicron MOS devices, a large electric field is unavoidable in some regions of the lateral channel. Therefore traditional drift-diffusion models are not adequate for describing its device characteristics. In order to account for a high-electric-field effect, the energy transport equation for analyzing the electron temperature distribution in the channel has been included in an analytical DC model for MOS transistors[2–4]. For deep submicron MOS devices designed with a large electron mobility, electrons in some region of its very short channel may be traveling at a velocity higher than the saturated velocity (the velocity overshoot phenomenon[5–9]). For a deep submicron NMOS device with velocity overshoot behavior, its device model is further complicated. Recently an analytical DC drain current formula for deep submicron NMOS devices considering velocity overshoot phenomenon has been reported and the effect of velocity overshoot on the drain current has been evaluated[10]. For a deep submicron MOS device, the drain current alone cannot describe the device performance. Capacitance is also very important in determining the overall performance of such a device. In the past MOS capacitance models have been discussed in-depth for transient analysis of MOS devices[11]. An analysis of capacitances in MOS devices considering velocity saturation has been reported[12]. However a capacitance model of a MOS device considering velocity

overshoot has not been reported. In this paper an analytical source-gate and drain-gate capacitance model considering velocity overshoot for a 0.1  $\mu\text{m}$  NMOS device is described. In the following sections, the derivation of the analytical model is described first, followed by a verification of the model and a discussion.

### 2. MODEL DERIVATION

In this section a velocity-overshoot capacitance model for a 0.1  $\mu\text{m}$  MOS device is derived. Consider a 0.1  $\mu\text{m}$  NMOS device with its origin at the source end and its  $y$ -axis in the lateral channel direction. In order to simplify the analysis, the gate fringing capacitance and the gate-source and the gate-drain overlap capacitances[13,14] are not considered. Based on the partitioned-charged capacitance model[11], the source charge and the drain charge are given by:

$$Q_{\text{S}} = W \int_0^L \left(1 - \frac{y}{L}\right) n(y) dy, \quad (1)$$

$$Q_{\text{D}} = W \int_0^L \frac{y}{L} n(y) dy, \quad (2)$$

respectively, where  $W$  is the width,  $L$  is the effective channel length and  $n(y)$  is the unit-area induced charge density at location  $y$  in the channel. Using eqns (1) and (2), the source-gate and drain-gate capacitances are defined as:

$$C_{\text{SG}} \equiv -\frac{\partial Q_{\text{S}}}{\partial V_{\text{G}}} \frac{1}{WL},$$

$$C_{\text{DG}} \equiv -\frac{\partial Q_{\text{D}}}{\partial V_{\text{G}}} \frac{1}{WL}, \quad (3)$$

\*To whom correspondence should be addressed.

respectively.

### 2.1. Energy transport

For an NMOS device the energy balance equation [15] is:

$$\frac{dS}{dy} = JE - 2n \frac{k(T_n - T_0)}{\tau_e}, \quad (4)$$

where  $y$  is the lateral direction,  $J$  is the electron current density,  $E$  is the lateral electric field,  $k$  is the Boltzmann constant,  $T_n$  is the electron temperature,  $T_0$  is the ambient temperature,  $n$  is the electron density,  $\tau_e$  is the energy relaxation time,  $S$  is the electron energy flux and  $2kT_n$  is the average kinetic energy per electron arising from current flow. The electron energy flux is expressed as:

$$S = -\kappa \frac{dT_n}{dy} - 2J \frac{kT_n}{q}, \quad (5)$$

where  $\kappa$  is the thermal conductivity,  $q$  is the electron charge. In the NMOS device the electron current, which is mainly composed of drift current, is:

$$J = nq\mu_n(T_n)E, \quad (6)$$

where  $\mu_n(T_n)$  is the temperature-dependent electron mobility[15]:

$$\mu_n(T_n) = \mu_s \left( \frac{T_n}{T_0} \right)^{-0.5}, \quad (7)$$

where  $\mu_s$  is the surface electron mobility[16]:

$$\mu_s = \frac{\mu_0}{1 + \theta(V_G - V_T)}.$$

From eqns (4)–(7) by neglecting the second order derivative term, one obtains a differential equation in terms of the electron temperature:

$$\frac{dT_n}{dy} = -\frac{qE}{2k} + \frac{(T_n - T_0)}{\tau_e \mu_s E} \left( \frac{T_n}{T_0} \right)^{0.5}. \quad (8)$$

However, at steady state, the electron mobility is also field dependent[17]:

$$\mu_n(E) = \frac{\mu_s}{\left[ 1 + \left( \frac{\mu_s E}{v_{sat}} \right)^2 \right]^{1/2}}, \quad (9)$$

where  $v_{sat}$  is the electron saturated velocity[18]:

$$v_{sat} = \frac{2.4 \times 10^7}{1 + 0.8 \times \exp(T_0/600)} \text{ (cm sec}^{-1}\text{)}. \quad (10)$$

At steady state the electron temperature dependent mobility is equal to the electric-field dependent mobility ( $\mu_n(T_{nss}) = \mu_n(E)$ ). Therefore from eqns (7) and (9), the steady-state electron temperature is:

$$T_{nss} = T_0 \left[ 1 + \left( \frac{\mu_s E}{v_{sat}} \right)^2 \right]. \quad (11)$$

Since the energy relaxation time is related to the difference between the steady-state electron temperature ( $T_{nss}$ ) and the ambient temperature and the electric field, as for instance

$$\tau_e = \frac{2k(T_{nss} - T_0)}{qEv_{ss}}, \quad (12)$$

from eqns (11) and (12) one obtains:

$$\tau_e = \frac{2kT_0\mu_s^2}{q\mu_n(E)v_{sat}^2} = \frac{2kT_0\mu_s^2}{q\mu_n(T_n)v_{sat}^2}. \quad (13)$$

Next from eqns (13) and (8) a differential equation in terms of the electron temperature is obtained:

$$\frac{dT_n}{dy} = -\frac{qE}{2k} + \frac{(T_n - T_0)qv_{sat}^2}{2kT_0E\mu_s^2}. \quad (14)$$

The electric field in the lateral channel between source and the saturation point has been assumed to be linear:

$$E(y) = E_0 + ay, \quad (15)$$

where  $E_0$  and  $a$  are defined as:

$$E_0 = -\frac{\eta V_{DSAT}}{L - \Delta L},$$

$$a = -\frac{2(1 - \eta)V_{DSAT}}{(L - \Delta L)^2}. \quad (16)$$

From eqns (14) and (15) in this case one obtains:

$$\frac{dT_n}{dy} = -\frac{q(E_0 + ay)}{2k} + \frac{(T_n - T_0)qv_{sat}^2}{2kT_0(E_0 + ay)\mu_s^2}. \quad (17)$$

Solving eqn (17) with the boundary condition that at the source end the electron temperature is equal to the ambient temperature ( $T_n(y=0) = T_0$ ), the distribution of the electron temperature in the lateral channel of the device is given by

$$T_n(y) = T_0 + \frac{B}{A + 2} (E_0 + ay)^2 \left[ 1 - \left( \frac{E_0}{E_0 + ay} \right)^{A+2} \right],$$

$$A = -\frac{qv_{sat}^2}{2akT_0\mu_s^2},$$

$$B = -\frac{q}{2ak}. \quad (18)$$

As  $\eta$  is small,  $(E_0/E_0 + ay)^{A+2}$  can be neglected. Therefore the electron temperature distribution becomes:

$$T_n(y) \cong T_0 + \frac{B}{A + 2} (E_0 + ay)^2. \quad (19)$$

### 2.2. Drain current

Using Ref.[19], the drain current is given by

$$I_D = \mu_{eff} C_{ox} \frac{W}{L - \Delta L} [(V_{GS} - V_T)V_{DX} - \frac{1}{2}V_{DX}^2], \quad (20)$$

where  $V_T$  is the threshold voltage considering drain induced barrier lowering effect:  $V_T = V_{i0} - \sigma V_{DS}$ , where  $V_{i0}$  is the zero bias threshold voltage,  $\sigma$  is a coefficient.  $\mu_{eff}$  is the effective electron mobility. Using a unified formula for both triode and saturation regions,  $V_{DX}$  is organized as:

$$V_{DX} = V_{DS} + V_{DSAT} - (V_{DS}^3 + V_{DSAT}^3)^{1/3}. \quad (21)$$

From eqn (21), in the triode region,  $V_{DX} \rightarrow V_{DS}$ . In the saturation region,  $V_{DX} \rightarrow V_{DSAT}$ , where  $V_{DSAT}$  is defined as:

$$V_{DSAT} = \frac{V_{DSAT1} V_P}{V_{DSAT1} + V_P}, \quad (22)$$

in which  $V_P$  is determined by the pinchoff point: ( $V_P = V_G - V_T$ ), and  $V_{DSAT1}$  is determined by the velocity saturation point. As the drain voltage reaches  $V_D = V_{DSAT1}$ , the electric field at the drain equals

$$E(y=L) = \frac{-(2-\eta)V_{DSAT1}}{L}. \quad (23)$$

Using the electron temperature profile formula (eqn (19)), eqn (28) becomes

$$\mu_{\text{eff}} = \frac{\mu_s T_0^{1/2} (L - \Delta L)}{\int_0^{L-\Delta L} \sqrt{T_0 + \frac{B}{A+2} (E_0 + ay)^2} dy}. \quad (29)$$

Finally by carrying out the integral of eqn (29) the effective electron mobility becomes:

$$\mu_{\text{eff}} = \frac{\sqrt{\frac{A+2}{B}} a \mu_s T_0^{1/2} (L - \Delta L)}{\left[ \frac{E}{2} \sqrt{E^2 + \frac{T_0(A+2)}{B}} + \frac{T_0(A+2)}{2B} \ln \left( E + \sqrt{E^2 + \frac{T_0(A+2)}{B}} \right) \right]_{E=E(y=0)}^{E=E(y=L-\Delta L)}}, \quad (30)$$

Under this condition, the electron velocity at the drain just reaches the saturated velocity. Therefore

$$\begin{aligned} \mu_n(E(y=L))|E(y=L)| \\ = \frac{\mu_s |E(y=L)|}{\sqrt{1 + \left( \frac{\mu_s E(y=L)}{v_{\text{sat}}} \right)^2}} = \eta_1 v_{\text{sat}}. \end{aligned} \quad (24)$$

According to eqns (23) and (24)  $V_{DSAT1}$  becomes:

$$V_{DSAT1} = \frac{\eta_1 v_{\text{sat}} L}{(2-\eta)\sqrt{1-\eta_1^2 \mu_s}}. \quad (25)$$

From Ref.[3] the distance between the saturation point and drain is found to equal

$$E(y=L-\Delta L) = -\frac{(2-\eta)V_{DX}}{L-\Delta L}. \quad (31)$$

### 2.3. Capacitances

Based on the drain current model and the partitioned-charge model, the source-gate and drain-gate capacitances of the 0.1 μm NMOS device are derived in this section.

The lateral channel is divided into two sections: (1) the pre-saturation section ( $0 < y < L - \Delta L$ ), and (2) the post-saturation section ( $L - \Delta L < y < L$ ). There-

$$\begin{aligned} \Delta L &= s\lambda \ln \left[ \frac{-(V_{DS} - V_{DX} - a_1 \lambda^2) - \sqrt{(V_{DS} - V_{DX} - a_1 \lambda^2)^2 + \lambda^2 (E_1^2 - a_1^2 \lambda^2)}}{\lambda (E_1 + a_1 \lambda)} \right], \\ \lambda &= \sqrt{\frac{\epsilon_{\text{Si}} x_j t_{\text{ox}}}{\epsilon_{\text{ox}}}}, \\ a_1 &= -\frac{2(1-\eta)V_{DX}}{L^2}, \\ E_1 &= -\frac{\eta V_{DX}}{L}. \end{aligned} \quad (26)$$

Since in the triode region  $V_{DX} \rightarrow V_{DS}$ ,  $\Delta L \rightarrow 0$ .

The effective electron mobility is expressed as:

$$\mu_{\text{eff}} = \frac{L - \Delta L}{\int_0^{L-\Delta L} \frac{1}{\mu_n} dy}. \quad (27)$$

From eqns (7) and (27) by considering the electron temperature distribution in the channel the effective mobility is expressed as:

$$\mu_{\text{eff}} = \frac{\mu_s (L - \Delta L)}{\int_0^{L-\Delta L} \left( \frac{T_n}{T_0} \right)^{1/2} dy}. \quad (28)$$

fore,  $Q_S$  and  $Q_D$  as indicated in eqns (1) and (2) can be expressed as:

$$Q_S = Q_{S1} + Q_{S2}, \quad (32)$$

$$Q_D = Q_{D1} + Q_{D2}, \quad (33)$$

where  $Q_{S1}$  and  $Q_{D1}$  are defined as:

$$Q_{S1} = W \int_0^{L-\Delta L} \left( 1 - \frac{y}{L} \right) n(y) dy, \quad (34)$$

$$Q_{D1} = W \int_0^{L-\Delta L} \frac{y}{L} n(y) dy, \quad (35)$$

and  $Q_{S2}$  and  $Q_{D2}$  are defined as:

$$Q_{S2} = W \int_{L-\Delta L}^L \left(1 - \frac{y}{L}\right) n(y) dy, \quad (36)$$

$$Q_{D2} = W \int_{L-\Delta L}^L \frac{y}{L} n(y) dy. \quad (37)$$

**2.3.1. Pre-saturation region.** In the presaturation region ( $0 \leq y \leq L - \Delta L$ ), the unit-area charge density at location  $y$  in the channel is:

$$n(y) = -C_{ox}(V_G - V_T - V(y)), \quad (38)$$

where  $V(y)$  is the potential at location  $y$  in the channel. Using the channel electric field distribution formula as shown in eqn (15), the channel potential becomes:

$$V(y) = \int_0^y -(E_0 + ay') dy' = -E_0 y - \frac{1}{2} ay^2. \quad (39)$$

From eqns (34, 35, 38 and 39), one obtains  $Q_{S1}$  and  $Q_{D1}$  in the presaturation region to equal

$$Q_{S1} = -C_{ox} W \left[ (V_G - V_T)(L - \Delta L) + \frac{1}{2} \left( E_0 - \frac{V_G - V_T}{L} \right) (L - \Delta L)^2 + \frac{1}{3} \left( \frac{1}{2} a - \frac{E_0}{L} \right) (L - \Delta L)^3 - \frac{1}{8} \frac{a}{L} (L - \Delta L)^4 \right], \quad (40)$$

$$Q_{D1} = -C_{ox} \frac{W}{L} \left[ \frac{1}{2} (V_G - V_T)(L - \Delta L)^2 + \frac{1}{3} E_0 (L - \Delta L)^3 + \frac{1}{8} a (L - \Delta L)^4 \right]. \quad (41)$$

**2.3.2. Post-saturation region.** In the post-saturation region ( $L - \Delta L \leq y < L$ ), the electrons are travelling at the velocity at the saturation point

Table 1. Parameters of the device under study

Parameter	Value
$L$	0.09 $\mu\text{m}$
$V_{t0}$	0.2 V
$s$	0.35
$t_{ox}$	75 $\text{\AA}$
$\eta$	0.1
$\eta_1$	0.94
$\mu_0$	450 $\text{cm}^2 \text{V}^{-1} \text{sec}^{-1}$
$x_j$	0.11 $\mu\text{m}$
$\sigma$	0.12

( $y = L - \Delta L$ ). From eqn (31), at the saturation point ( $y = L - \Delta L$ ), the electric field is:

$$E(y = L - \Delta L) = -\frac{(2 - \eta)V_{DX}}{L - \Delta L}. \quad (42)$$

From eqn (19), at the saturation point ( $y = L - \Delta L$ ), the electron temperature is:

$$T_n(y = L - \Delta L) = T_0 + \frac{B}{A + 2} (E(y = L - \Delta L))^2. \quad (43)$$

From eqn (7), at the saturation point ( $y = L - \Delta L$ ), the electron velocity is

$$v_n(y = L - \Delta L) = \mu_s \left( \frac{T_n(y = L - \Delta L)}{T_0} \right)^{-0.5} E(y = L - \Delta L). \quad (44)$$

In the post-saturation region, the effective charge density is  $n(y) = (I_D / W v_n(y = L - \Delta L))$ . Therefore from eqns (36, 37, 44) one obtains:

$$Q_{S2} = \frac{I_D \Delta L^2}{2L v_n(y = L - \Delta L)}, \quad (45)$$

$$Q_{D2} = \frac{I_D}{v_n(y = L - \Delta L)} \left( \Delta L - \frac{\Delta L^2}{2L} \right). \quad (46)$$

Eqns (1-3, 32, 33, 40, 41, 45, 46) are closed-form analytical  $C_{SG}$  and  $C_{DG}$  formulas for the 0.1  $\mu\text{m}$  NMOS device considering velocity overshoot.

### 3. MODEL VERIFICATION

In order to evaluate the effectiveness of the analytical velocity overshoot model, the analytical model results for  $C_{SG}$  and  $C_{DG}$  have been compared to 2D simulation results[20]. As shown in Table 1, the NMOS device under study has an effective channel length of 0.09  $\mu\text{m}$ , a gate oxide thickness of 75  $\text{\AA}$  and a  $S/D$  junction depth of 0.11  $\mu\text{m}$ . The zero bias threshold voltage of the device is 0.2 V.

Figure 1 shows the electron drift velocity distribution in the lateral channel direction of the NMOS device biased at  $V_D = 1 \text{ V}$  and  $V_G = 1.0 \text{ V}$ , based on the 2D simulation results and on the analytical velocity overshoot model.  $\mu_0 = 450 \text{ cm}^2 \text{ v sec}^{-1}$ . As shown in the figure, the electron drift velocity distribution of the model result is well correlated to the 2D simulation result. At  $V_D = 1 \text{ V}$  and  $V_G = 1.0 \text{ V}$ , in

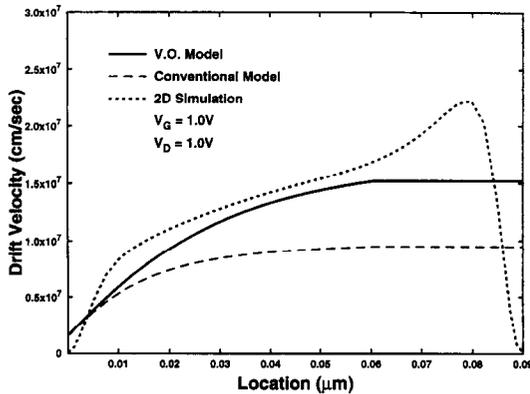


Fig. 1. Electron drift velocity distribution in the lateral channel direction of the NMOS device biased at  $V_D = 1 \text{ V}$  and  $V_G = 1.0 \text{ V}$ , according to 2D simulation results, the analytical velocity overshoot model, and the conventional model, respectively.  $\mu_0 = 450 \text{ cm}^2 \text{ V}^{-1} \text{ sec}^{-1}$ .

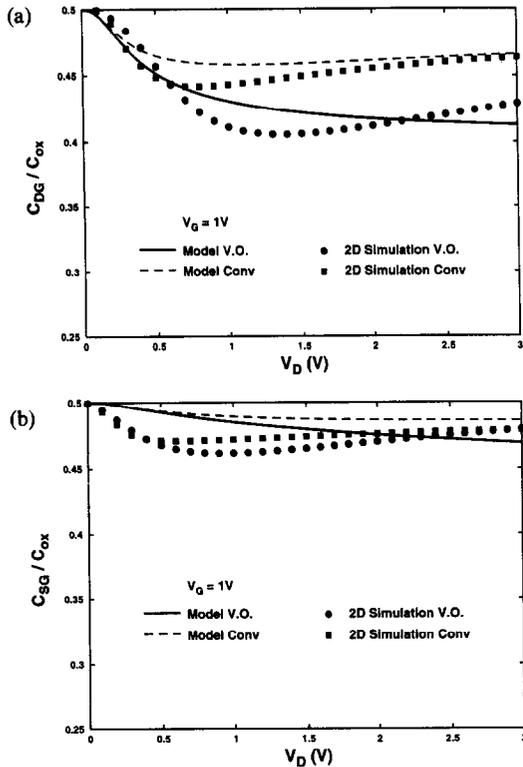


Fig. 2. (a)  $C_{DG}$  and (b)  $C_{SG}$  vs  $V_D$  of the NMOS device with a channel length of  $0.09 \mu\text{m}$ , biased at  $V_G = 1 \text{ V}$ , based on the analytical model considering velocity overshoot and without considering it, and 2D simulation results, respectively.

most parts of the lateral channel, the drift velocity is higher than the saturated velocity ( $10^7 \text{ cm sec}^{-1}$ ). Using the analytical velocity overshoot model, velocity overshoot behavior can be observed. However using the conventional model, velocity overshoot behavior cannot be identified.

Figures 2(a) and 2(b) show  $C_{DG}$  and  $C_{SG}$  vs  $V_D$  of the NMOS device (biased at  $V_G = 1 \text{ V}$ ) according to both analytical models and 2D simulation. As shown in the figures, at small  $V_D$  with and without considering velocity overshoot, a similar result can be observed for both  $C_{SG}$  and  $C_{DG}$ . When  $V_D$  becomes large, a difference in  $C_{SG}$  and  $C_{DG}$  with and without considering velocity overshoot becomes noticeable. Compared to  $C_{SG}$ , the difference in  $C_{DG}$  with and without considering velocity overshoot is larger. Specifically at large  $V_D$ , considering velocity overshoot  $C_{DG}$  degrades more. The trends in  $C_{DG}$  and  $C_{SG}$  predicted by the analytical model are confirmed by the 2D simulation results.

#### 4. DISCUSSION

The larger decrease in  $C_{DG}$  when considering velocity overshoot can be understood by considering

$C_{DG1}$ ,  $C_{DG2}$ ,  $C_{SG1}$  and  $C_{SG2}$ , which in the pre-saturation region are defined as

$$C_{DG1} \equiv -\frac{\partial Q_{D1}}{\partial V_G} \frac{1}{WL}, \quad C_{SG1} \equiv -\frac{\partial Q_{S1}}{\partial V_G} \frac{1}{WL};$$

and in the post-saturation region as

$$C_{DG2} \equiv -\frac{\partial Q_{D2}}{\partial V_G} \frac{1}{WL}, \quad C_{SG2} \equiv -\frac{\partial Q_{S2}}{\partial V_G} \frac{1}{WL}.$$

Note that  $C_{DG1} + C_{DG2} = C_{DG}$ ,  $C_{SG1} + C_{SG2} = C_{SG}$ .

Figures 3(a) and 3(b) show the normalized value of  $C_{DG1}$  and  $C_{DG2}$  and  $C_{SG1}$  and  $C_{SG2}$  vs  $V_D$  of the NMOS device, biased at  $V_G = 1 \text{ V}$ , based on both analytical models. As shown in Fig. 3(a), when  $V_D$  is small,  $C_{DG1}$  for the pre-saturation region is much larger than  $C_{DG2}$  for the post-saturation region. When  $V_D$  becomes large,  $C_{DG2}$  for the post-saturation region is much larger than  $C_{DG1}$ . In the pre-saturation region, with and without considering velocity overshoot,  $C_{DG1}$  is identical. In contrast, in the post-saturation region, considering velocity overshoot,  $C_{DG2}$  is smaller when compared to the case without considering it. This is correlated to the results shown in Fig. 2(a). As shown in Fig. 3(b) regardless of  $V_D$   $C_{SG1}$  for the presaturation region is always much larger than  $C_{SG2}$  for the post-saturation region. In the pre-saturation region, with and without considering

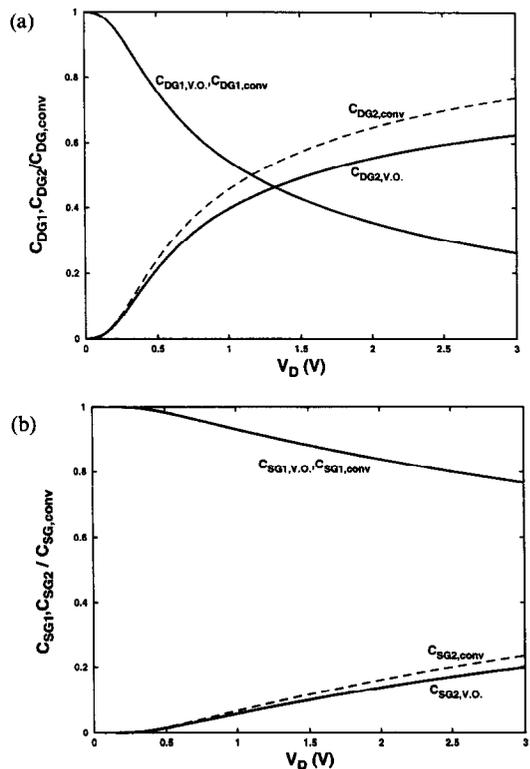


Fig. 3. (a) Normalized  $C_{DG1}$  and  $C_{DG2}$  and (b) normalized  $C_{SG1}$  and  $C_{SG2}$  vs  $V_D$  of the NMOS device with a channel length of  $0.09 \mu\text{m}$ , biased at  $V_G = 1 \text{ V}$ , based on the analytical model considering velocity overshoot and without considering it, respectively.

velocity overshoot,  $C_{SG1}$  is identical. In the post-saturation region, considering velocity overshoot  $C_{SG2}$  is smaller when compared to the case without considering it. From Figs 3(a) and 3(b), we learn that for  $C_{SG}$  the pre-saturation region is more important— $C_{SG1}$  is more important than  $C_{SG2}$ . Considering velocity overshoot, in the post-saturation region, when  $V_D$  is large,  $C_{SG2}$  may become smaller than that without considering it. Since  $C_{SG1}$  of the presaturation region always dominates  $C_{SG}$ , at large  $V_D$ , the decrease in  $C_{SG2}$  of the post-saturation region when considering velocity overshoot only makes  $C_{SG}$  decrease a little bit. However, for  $C_{DG}$ , the post-saturation region can be more important—at large  $V_D$ ,  $C_{DG2}$  is more important than  $C_{DG1}$ . Therefore at large  $V_D$  the decrease in  $C_{DG2}$  of the post-saturation region when considering velocity overshoot makes  $C_{DG}$  decrease much more when compared to the  $C_{SG}$  case. This explains the larger decrease in  $C_{DG}$  when considering velocity overshoot at large  $V_D$  when compared to the  $C_{SG}$  case. The decrease in  $C_{DG2}$  in the post-saturation region when considering velocity overshoot at large  $V_D$  is caused by a larger electron drift velocity in the post-saturation region.

## 5. CONCLUSION

In this article the impact of velocity overshoot on the source-gate and drain-gate capacitance in a  $0.1\ \mu\text{m}$  NMOS device has been discussed. As verified by 2D simulation results, based on the analytical capacitance model considering velocity overshoot, since a smaller amount of electrons exists in the channel region  $C_{SG}$  and  $C_{DG}$  show a smaller value when compared with the conventional model. As compared to the  $C_{SG}$  case, the larger decrease in  $C_{DG}$  when considering velocity overshoot at high  $V_D$  is the result of higher electron velocity in the post-saturation region.

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