

## A MODIFIED BOW-TIE SLOT ANTENNA FED BY A COPLANAR WAVEGUIDE

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A modified CPW-fed bow-tie slot antenna is proposed to have a wider impedance bandwidth than that of the conventional CPW-fed bow-tie slot antenna. The antenna structure remains simple and the better impedance matching is obtained through the insertion of a 180-degree delay slotline between the feeding CPW and one of the two parts of the bow-tie slot. A 47.4% impedance bandwidth, 2.3 to 5.1 dBi in-band antenna gains, and broadside bi-directional radiation patterns are measured and presented for an H-band prototype antenna.

### 1. Introduction

The bow-tie slot antenna is a broadband design conventionally used in many communication applications [1]-[5]. However, the operating bandwidth is never wide enough for the increasing capacity and data rate demands of modern communication systems. In order to have an even broader bandwidth while maintaining a simple structure, a novel bandwidth-enhanced bow-tie slot antenna fed by a coplanar waveguide (CPW) is proposed in this paper. An H-band prototype is verified experimentally to have a wider bandwidth than that of the conventional design.

### 2. Antenna Structure

The configurations of the conventional CPW-fed bow-tie slot antenna and the present proposed bandwidth-enhanced design are shown in Figs. 1(a) and (b), respectively. Both antennas have simple structures with only one layer of dielectric substrate and metalization. The geometry of the conventional CPW-fed bow-tie slot antenna is symmetrical to the direction of the feedline, while the proposed bandwidth-enhanced design is not. The conventional design is broadband and its radiation patterns near resonance resemble those of a slot dipole antenna. The outer width of the bow-tie slot  $W$  can be tuned for the input matching at the operating frequency, and the total length of the bow-tie slot  $2L$  determines the resonant frequency  $f_0$  with  $2L=\lambda_0$ . In our proposed design as shown in Fig. 1(b), a 180-degree delay slotline is inserted between the CPW feedline and the right hand side (RHS) part of the bow-tie slot. This will make the equivalent magnetic currents flowing on the two sides of the bow-tie slot out of phase, and thus, results in a cancellation in the broadside radiation. In

order to avoid this, we flip the delayed RHS part of the bow-tie slot over to the other side of the connecting slotline. This provides an additional 180-degree spatial phase difference to maintain in-phase magnetic current distributions on the two sides of the bow-tie slot. The 180-degree delay line possessing two orthogonal slotline sections,  $L_1$  and  $L_2$ , ensures a compact antenna size and further increases the impedance bandwidth.

### 3. Simulation and Measurement Results

During the design process, the length of one half of the bow-tie slot  $L$  is first determined to be  $\lambda_0/2$  at the required center frequency  $f_0$  just as in the case of the conventional bow-tie slot antenna. Note that the outer width of the bow-tie slot  $W$  of the proposed design is smaller than that of the conventional one. The total length of the delay slotline,  $L_1+L_2$ , should be slightly less than  $\lambda_0/2$ , and  $L_2$  is recommended to be longer than two times of  $L_1$ . Throughout the design process, simulations are carried out on a package software Ensemble [6] from Ansoft.

A test piece is fabricated on an FR-4 substrate with dielectric constant  $\epsilon_r = 4.3$  and thickness of 1.6 mm, and is designed to operate at 4.5 GHz. The design parameters are as follows:  $L=25$  mm,  $W=12$  mm,  $w=0.3$  mm,  $L_1=6$  mm, and  $L_2=14.7$  mm. The widths of the strip and slot of the 50- $\Omega$  CPW feedline,  $S$  and  $G$ , are chosen to be 3 mm and 0.3 mm, respectively. Moreover, a conventional CPW-fed bow-tie slot antenna with optimized bandwidth is also implemented on the same substrate and tested for comparison. Measured return losses of both cases are shown in Fig. 2. The measured impedance bandwidths (Return loss > 10 dB) of the optimized conventional design and the present design are 38.6% and 47.4%, respectively. An improvement of about 23% for the impedance bandwidth is achieved with our design. The radiation patterns of the bandwidth-enhanced design measured at 3.5, 4.2, 5.3 and 5.7 GHz are shown in Figs. 3(a), (b), (c), and (d), respectively. The radiation patterns of the present design remain satisfactory throughout the entire frequency band, and the antenna gains measured at these four frequencies are 3.5, 3.4, 5.1 and 2.3 dBi, respectively.

### 4. Conclusion

The design of a bandwidth-enhanced bow-tie slot antenna fed by a CPW has been presented. This design demonstrates a much wider impedance bandwidth than that of the conventional CPW-fed bow-tie slot antenna. The in-band radiation patterns remain broadside and bi-directional. In addition, this antenna preserves several advantages as in the case of the conventional one, such as ease of fabrication and design, and compact in size, and it can find many applications in the integration of mobile communications.

### Acknowledgements

This work is supported in part by the National Science Council, Republic of China, under contract no. NSC 92-2219-E-002-002, and in part by the Ministry of Education, ROC, under contract no. 89-E-FA06-2-4.

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- [6] Trade mark of Ansoft Corp.

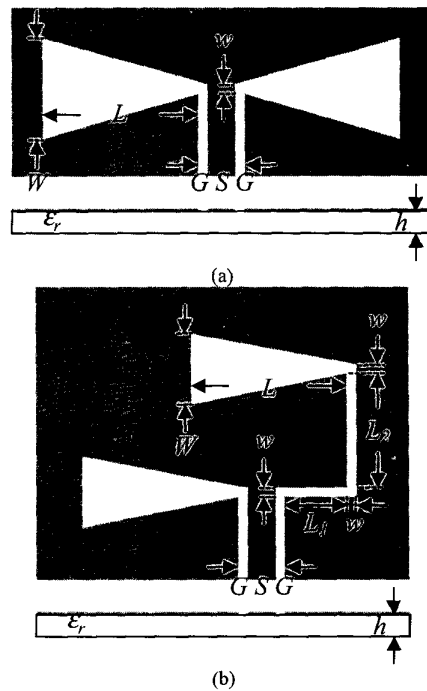


Fig. 1. Geometries of (a) conventional CPW-fed bow-tie slot antenna and (b) bandwidth-enhanced CPW-fed bow-tie slot antenna.

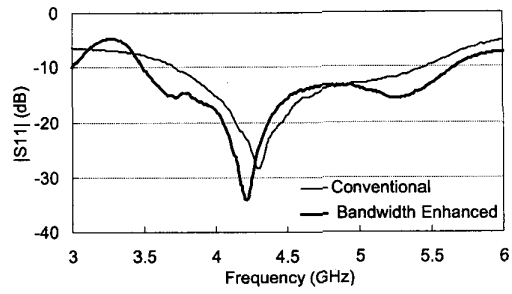


Fig. 2. Measured input return losses of the conventional CPW-fed bow-tie slot antenna and the bandwidth-enhanced CPW-fed bow-tie slot antenna.

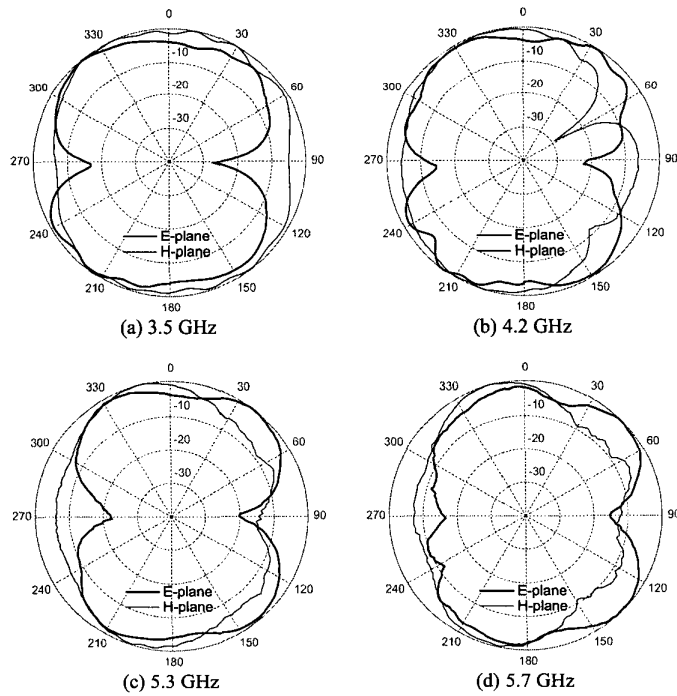


Fig. 3. Radiation patterns measured at 3.5, 4.2, 5.3 and 5.7 GHz of the H-band prototype.