Figure 3(a) shows the SOA bias current dependence of the recovery time. The probe wavelength is fixed at 1550 nm and ECL output power is at 5.5 dBm. The gain recovery time changes from 45 ps to 13 ps corresponding to bias current from 200 mA to 700 mA. Afterwards the speed is limited by the resolution of our measurement setup. Figure 3(b) shows the probe wavelength dependence of gain recovery time at a constant injection current (I = 600 mA). The ECL output power is kept at 3 dBm when operated at different wavelength. With constant input powers for both the pump and probe, the gain recovery is fastest at the device gain peak and slower at the higher and lower wavelengths. This again shows that to increase the SOA gain is essential to obtain very high speed all optical operations. The proposed two-section operation makes it possible to easily obtain  $\sim$  100 Gbit/s all optical devices.

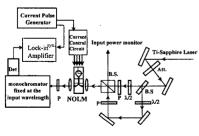
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## CTuK20

## Wavelength dependence and cross polarization effects of nonlinear switching in an all-semiconductoroptical-amplifier loop device

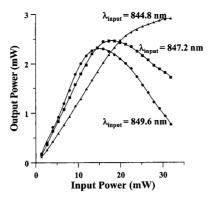
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We report the experimental and simulation results of the wavelength dependence and cross polarization effects of nonlinear switching in an all-semiconductor-optical-amplifier loop device. For input/output coupling, a multimode interference (MMI) amplifier was connected to the loop. The observed nonlinear



P: polarizer λ/2: half wave plate B.S.: beam splitter Att. attenuator

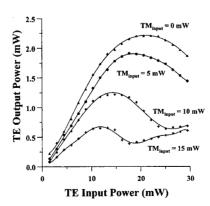
CTuK20 Fig. 1. Experimental setup for non-linear switching measurements.



CTuK20 Fig. 2. Output power as a function of input power (the value before entering the waveguide) at different wavelengths in the TE polarization.

switching comes from the combined effect of the nonlinear coupling in the MMI amplifier and the lateral wave field redistribution caused by the loop. This mechanism is different from that in a nonlinear optical loop mirror in which the nonlinear optical mechanism comes from the loop. Our device has a loop of 300 µm in radius, which is formed with a curved ridgeloading waveguide with a ridge width 4 µm. The loop is connected to an MMI waveguide with a length 460 or 500 µm and a ridge width 8 µm. This MMI waveguide serves the function of a coupler. Then, the input and output legs are formed with 4 µm wide waveguides. Both have the lengths of about 100 µm. The semiconductor optical amplifiers were fabricated on a four-period GaAs/AlGaAs multiple quantum well epitaxial structure. The fabrication procedures were the same as the typical processes for semiconductor lasers except the use of the UV-assisted cryo-etching technique for forming high-quality ridge-loading waveguides. For injecting different currents into different areas, we divided the electro-pad into four disconnected regions.

Figure 1 shows the experimental setup for our nonlinear switching measurements. A cw Ti:sapphire laser was used for providing the degenerate pump and signal. The coupling ef-



CTuK20 Fig. 3. Output power as a function of input TE signal power (the value before entering the waveguide) with different input TM signal power levels (0, 5, 10 and 15 mW for the curves from the top to bottom).

ficiency of laser into the device waveguide was estimated to be lower than 0.1%. A monochromator fixed at the input wavelength with a window of 2 nm was placed after the device for collecting signal power. Figure 2 shows the nonlinear switching results at different input wavelengths. We can see that at 849.6 nm, at which the electro-luminescence is the highest, the nonlinear switching is most efficient. At the other two wavelengths, a few nm lower than the maximum gain, nonlinear switching becomes less prominent. We observed the similar trend when we increased the wavelength from 849.6 nm. A larger separation of wavelength from this value led to a weaker nonlinear switching effect.

Figure 3 shows the nonlinear switching effect of the input TE signal with a cross-polarization modulation measurement. Here, the TM signal was set at 0, 5, 10 and 15 mW for the curves from the top to bottom. We can see that the input of the TM signal degrades the nonlinear switching of the TE signal. This result can be attributed to the fact that the consumption of carriers by the TM signal reduces the gain and the gain saturation effect of the TE signal. Such a phenomenon can be used for multiplexing/de-multiplexing. The nonlinear switching results with pulsed signals will also be discussed in this paper.

## CTuK21

## Giant optical nonlinearity and ultrafast carrier dynamics of a strained quantum well saturable Bragg reflector (SSBR)

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Recently, semiconductor saturable Bragg reflectors (SBRs) have been successfully developed for passive mode-locking of solid state lasers.1-3 In particular, we have developed a triple strained quantum well saturable Bragg reflector (SSBR) with saturation fluence as low as 12 µJ/cm<sup>2</sup>.4 This suggests potential applications of this device for applications such as all-optical swiching and modulation. In this work, we report a new type of SBR using triple strained-layer quantum wells as the absorbing laver which named strained saturated bragg reflector (SSBR). Because of it's low saturation energy and large tunning range, we want to understand the carrier dynamics with detailed wavelength. The time-resolved differention reflection  $(\Delta R/R)$  in this SSBR with detailed varient pumping energies have been observed. The influence of carrier scattering and process of recombination on the temperal and spectral  $\Delta R/R$  dynamics have been investigated.

The structure, reflectivity and photoluminescence spectra of the SSBR are shown in Fig. 1. Femtosecond pump/probe experiments were performed. The normalized time-resolved reflectivity,  $\Delta R/R$ , of the SSBR sample as a function of the pumping wavelength are shown in Fig. 2. The wavelength-dependent peak values of  $\Delta R/R$  are plotted in Fig. 3. When the sample was excited at a photon energy above the band gap ( $\lambda < 757.5$  nm),  $\Delta R/R$  is positive and with