



Sorption and diffusion of supercritical carbon dioxide in polycarbonate

Muoi Tang^{a,*}, Tz-Bang Du^b, Yan-Ping Chen^b

^a Department of Chemical Engineering, Chinese Culture University, Taipei, Taiwan, ROC

^b Department of Chemical Engineering, National Taiwan University, Taipei, Taiwan, ROC

Received 29 July 2002; received in revised form 7 February 2003; accepted 24 February 2003

Abstract

Sorption and diffusion of supercritical carbon dioxide (SCCO₂) in polycarbonate (PC) at temperatures ranged from 40 to 60 °C and pressures ranged from 10 to 40 MPa are presented in this study. The equilibrium CO₂ sorption in PC specimen with 0.5 mm thickness has been observed at 2 h, and the experimental data were analyzed by a mass-loss analysis. The linear relationship between mass gain and square root of time indicates that SCCO₂ conducted Fickian sorption and desorption in the PC specimen within the experimental conditions. The equilibrium CO₂ sorption amount in PC specimen varies from 7.6 wt.% (at 60 °C and 10 MPa) to 14.7 wt.% (at 40 °C and 40 MPa). Upon plotting the equilibrium sorption amounts against SCCO₂ density, crossover of the sorption isotherms is observed and the change of mass transfer mechanism is suggested. The sorption diffusivities under supercritical conditions as well as the desorption diffusivities under ambient temperature and pressure were determined. The sorption diffusivities increased with temperature and decreased with pressure of SCCO₂, unless the glass transition state of polymer was exceeded. The desorption diffusivities were also observed to increase with CO₂ concentration inside the PC specimen. At lower temperature and pressure, the desorption diffusivity may become larger than that of sorption due to the plasticizing effect.

© 2003 Elsevier B.V. All rights reserved.

Keywords: Diffusivity; Supercritical carbon dioxide; Polycarbonate

1. Introduction

The applications of supercritical carbon dioxide (SCCO₂) as a solvent or swelling agent in polymer chemistry are developing in recent years [1–10]. This fluid has conventional advantages for applications in green processes. It is also provided with plasticizing and swelling effects that can accelerate the

infusion of additives into a polymer substrate [3–10]. Operation of the supercritical fluid process is easily managed by adjusting the temperature and pressure. In our previous investigation, we used SCCO₂ as an impregnation solvent to synthesize conducting polymer composites of polypyrrole (PPy) with polymer substrates of polystyrene (PS) and polycarbonate (PC) [3–5]. It was indicated that the interactions of SCCO₂ with polymer substrates are important factors to the resulting conductivities. Different CO₂ sorption rates and hence the PPy contents in the composites

* Corresponding author. Fax: +886-2-2861-4011.

E-mail address: chemengtang@yahoo.com.tw (M. Tang).

were observed with different polymer substrates. These results suggest that the diffusion and sorption of SCCO₂ in polymers have to be investigated for further applications of SCCO₂ in polymer processing.

Various apparatus and methods have been employed to measure the diffusion coefficient and sorption amount of CO₂ in polymers [11–15]. Precise equipments such as the quartz spring or crystal microbalance were used [11,12] to measure the sorption amount, without experimental report at higher temperatures. Although a magnetic suspension balance was applied in high temperature measurements [15], only the equilibrium sorption amounts were generated. To provide explanation on the molecular interactions in polymer processing, further kinetic data and the sorption amounts at various time periods are also required.

Schnitzler et al. [10] studied the mass transfer of dispersed dyes in polyethyleneterephthalate (PET) using supercritical CO₂. Both the equilibrium and kinetic data were measured at temperatures up to 120 °C and pressures up to 35 MPa by a magnetic coupled balance. The gravimetric method was also applied to generate kinetic data by various authors [3,16–18]. The sorption amount was estimated by extrapolating the residual weight in the desorption process within a short time period. Applying reasonable assumption of Fickian diffusion, the experimentally measured desorption data were fitted by a linear equation to yield the sorption amount and the diffusion coefficients. In this method, the pressure vessel should be small to avoid venting a large volume of CO₂ under high pressure operation conditions. Otherwise, significant error is introduced in extrapolating the desorption data owing to a larger time period needed to transfer the sample to a balance. In this study, a small pressure vessel of 10 ml was employed in the measurement with a precise and dynamically controlled syringe pump. The desired pressure in the experiment was reached in a short period of 10 s. No problem of pressure drop was concerned, and the sample was easily taken out of the pressure vessel by hand screwing.

New data on the kinetic sorption amount and diffusion coefficient of SCCO₂ in PC, under pressures up to 40 MPa and temperatures up to 60 °C, were measured in this study. The sorption and desorption data of SCCO₂ at the experimental conditions were analyzed by the Fickian diffusion equation. The sorption isotherm, sorption and desorption diffusivities

are presented. Tensile tests were also performed to verify the plasticizing effect of SCCO₂ in PC.

2. Experimental

2.1. Materials

Pellets of PC (molecular weight 64 000, Acros) were hot pressed at 200 °C to obtain PC sheet with 0.5 mm thickness. The sheet was cut into the experimental specimen with dimensions of 40×12 mm. Carbon dioxide was purchased from San-Fu Chemical (Taiwan) with purity better than 99.5 mol%.

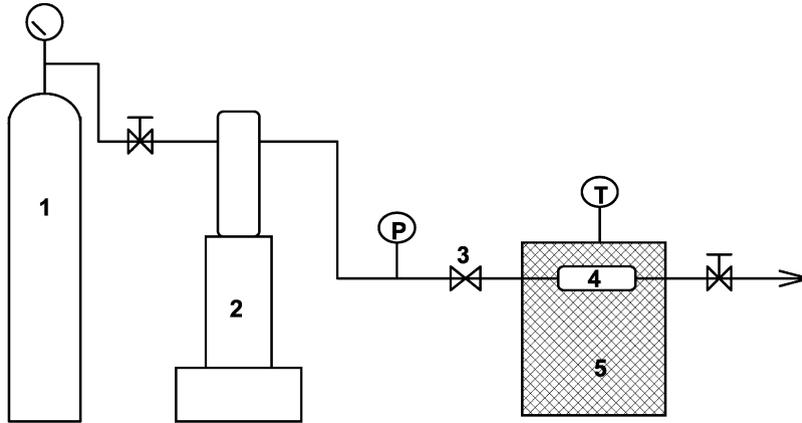
2.2. Experimental apparatus and procedures

The experimental apparatus is shown in Fig. 1. The high-quality CO₂ was compressed to the operating pressure by a syringe pump (ISCO, model 100DX). The compressed CO₂ flew into a column of 10 cm³, which was placed in a constant temperature bath (ISCO, SFX 2-10). The experimental temperature and pressure were dynamically controlled within the desired values.

The weighted polymer specimen was put into the high pressure column in the thermal bath at a controlled temperature. The pre-pressurized CO₂ in the syringe pump was flowing into the column within 10 s. The pressure in the column was dynamically controlled throughout the sorption process. After a period of sorption time, the column was rapidly vented and the specimen was transferred to a digital balance (Mettler AE200, sensitivity 0.1 mg) under room temperature at atmospheric pressure for desorption measurements. Generally, it took 30 s during the venting and weighting processes before the first data was recorded. The weight of specimen was recorded within 100 s at an interval of 10 s. As a consequence, eight data points have been reported for each experiment at a fixed temperature and pressure. These data points were used to determine the diffusivity for the sorption or desorption of CO₂ into or from the PC specimen.

2.3. Data analysis

The methods in analyzing the sorption and desorption data were described by previous investigators



- 1: CO₂ tank
- 2: high pressure syringe pump (ISCO 100DX)
- 3: non-return valve
- 4: high pressure column
- 5: thermostatted vessel (ISCO SFX 2-10)

Fig. 1. Schematic illustration of the experimental apparatus.

[16,18]. The governing equation was the basic mass transfer equation for a plane sheet system [19]:

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial X^2} \quad (1)$$

where C is the concentration and D is the diffusivity. One-dimensional diffusion along the thickness ℓ of the planar polymer and constant diffusivity were assumed in this study. Since the ratio of thickness to length of specimen is small, edge effect is also negligible [19]. With proper initial and boundary conditions [19] and the application of Laplace transform method, the following analytical solution was obtained:

$$\frac{M_t}{M_\infty} = 1 - \sum_{n=0}^{\infty} \frac{8}{(2n+1)^2 \pi^2} \exp\left(\frac{-D(2n+1)^2 \pi^2 t}{\ell^2}\right) \quad (2)$$

where M_t is the amount of sorption into the planar specimen at time t, M_∞ is equilibrium sorption amount and ℓ is the thickness of the specimen. Simplification of Eq. (2) by truncating at the first term in the

summation yields the following form for the longer time sorption process:

$$\frac{M_s}{M_\infty} = 1 - \frac{8}{\pi^2} \exp\left(\frac{-D_s \pi^2 t_s}{\ell^2}\right) \quad (3)$$

where M_s is the sorption amount at time t_s , expressed as the weight percentage of CO₂ per unit weight of polymer. M_∞ is the saturated sorption amount at a larger sorption time. A schematic illustration of the mass-loss analysis to evaluate the M_s and M_∞ values is demonstrated in Fig. 2. M_s was obtained by extrapolating the desorption amount M_d to the zero desorption time. M_d is the measured percentage weight loss during the desorption process. For a Fickian diffusion, M_d is a linear function of the square root of the desorption time t_d , and a linear fit gives M_s at zero t_d . Eq. (3) was then used to determine the sorption diffusivity D_s by plotting $\ln(1 - M_s/M_\infty)$ against (t_s/ℓ^2) .

The solution of Eq. (1) can also be expressed by a series expansion of error functions. This alternative solution has been directly introduced to analyze the desorption process after simplifying the equation at a

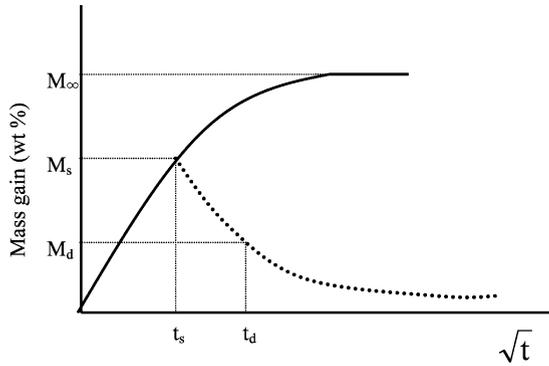


Fig. 2. Schematic illustration of the desorption measurement and mass-loss analysis.

small desorption time period [16,18]:

$$\frac{M_d}{M_\infty} = -\frac{4}{\ell} \sqrt{\frac{D_d t_d}{\pi}} \quad (4)$$

The desorption diffusivity D_d was thus determined by plotting (M_d/M_∞) against $(\sqrt{t_d}/\ell)$.

2.4. Characterization

The apparent changes of the specimen were examined directly using digital photograph. The yielding stress of the polymer specimen was measured using the tensile meter (RTM-1T) for verifying the plasticizing effect of CO_2 on polymer.

3. Results and discussion

3.1. Sorption of CO_2 into PC

The amount of sorption of CO_2 into PC specimen, M_s , was estimated by extrapolating the measured desorption weight fraction, M_d , to the zero desorption time. An example is shown in Fig. 3 for the desorption

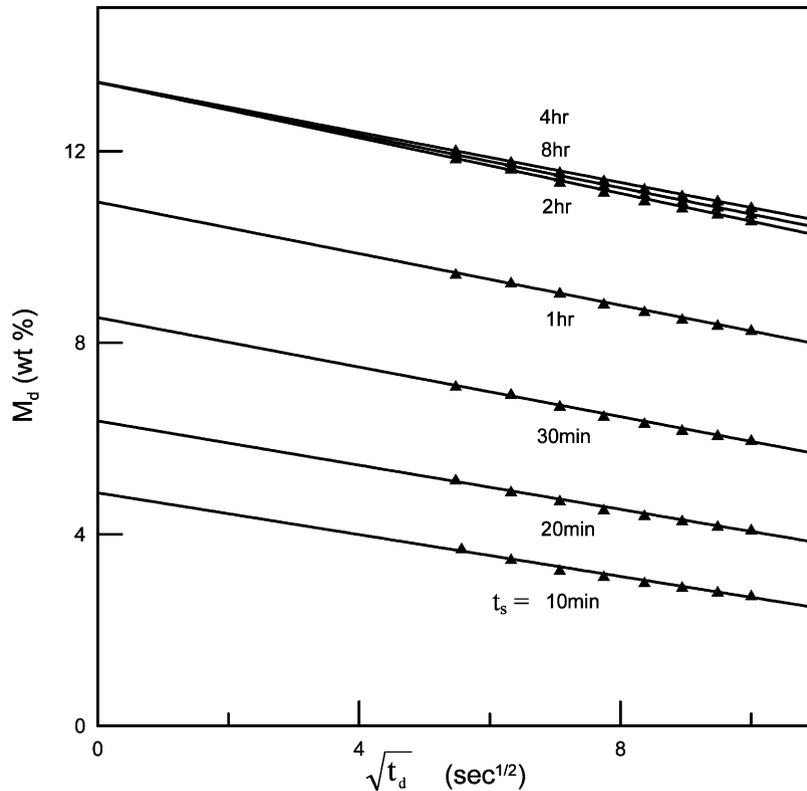


Fig. 3. Plot of the measured desorption weight fraction (M_d) against the square root of desorption time (t_d). PC specimen has been sorbed at 40°C and 30 MPa with various sorption times (t_s).

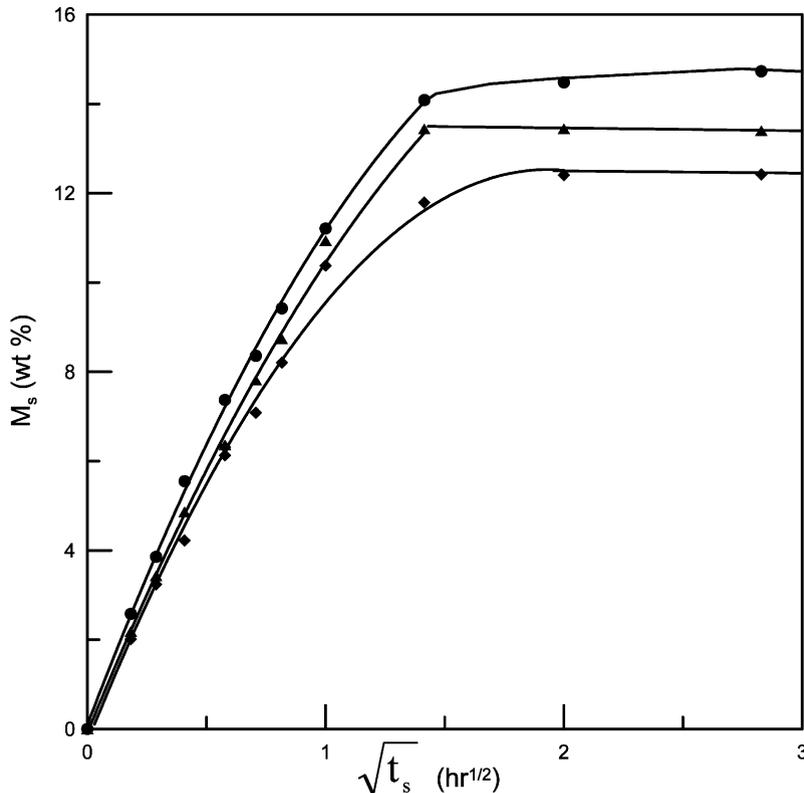


Fig. 4. Plot of the CO₂ sorption amount (M_s) against the sorption time (t_s) at 40 °C and various pressures: ◆, 20 MPa; ▲, 30 MPa; and ●, 40 MPa.

experiments at 40 °C and 30 MPa. The linear relationship between M_d and $\sqrt{t_d}$ at small desorption time period indicates that the assumption of Fickian diffusion is acceptable. The M_s values at various sorption times, t_s , are determined from the intercepts, and a sorption curve is then generated. Fig. 4 shows an example of the sorption curve at 40 °C where M_s values are plotted against $\sqrt{t_s}$ at various pressures. Initially, the M_s value increases linearly with $\sqrt{t_s}$, indicating that SCCO₂ conducted Fickian sorption into the PC specimen. The SCCO₂ sorption amount levels off after equilibrium is reached. In this study, equilibrium was reached around 2 h sorption time for PC specimen with 0.5 mm thickness at all experimental conditions. The equilibrium state sorption isotherms are shown in Fig. 5. The equilibrium sorption amounts, M_∞ , in Fig. 5 were obtained from the average leveling off values of M_s shown in Fig. 4 at each temperature and pressure. The M_∞ values shown in Fig. 5

increase with increasing pressure for each isotherm. They also decrease with increasing temperature at a fixed pressure. The largest M_∞ value reaches 14.7 wt.% at 40 °C and 40 MPa. The easier capillary condensation and trapping of SCCO₂ inside a polymeric matrix at a lower temperature and a higher pressure lead to this result. The same trend has been observed in the investigation of the sorption and diffusion of SCCO₂ in poly (vinyl chloride) [18]. Furthermore, the M_∞ values are plotted against the density of SCCO₂, as shown in Fig. 6. The crossover of isotherms is observed. At lower densities, the SCCO₂ solubility in PC decreases with increasing temperature. At higher densities, however, the CO₂ solubility increases with increasing temperature. The same relation is also found for the mass transfer in poly (ethylene terephthalate) [10]. It has been suggested that a change in the mass transfer mechanism occurred. At lower densities, dual mode sorption dominates where SCCO₂ was absorbed

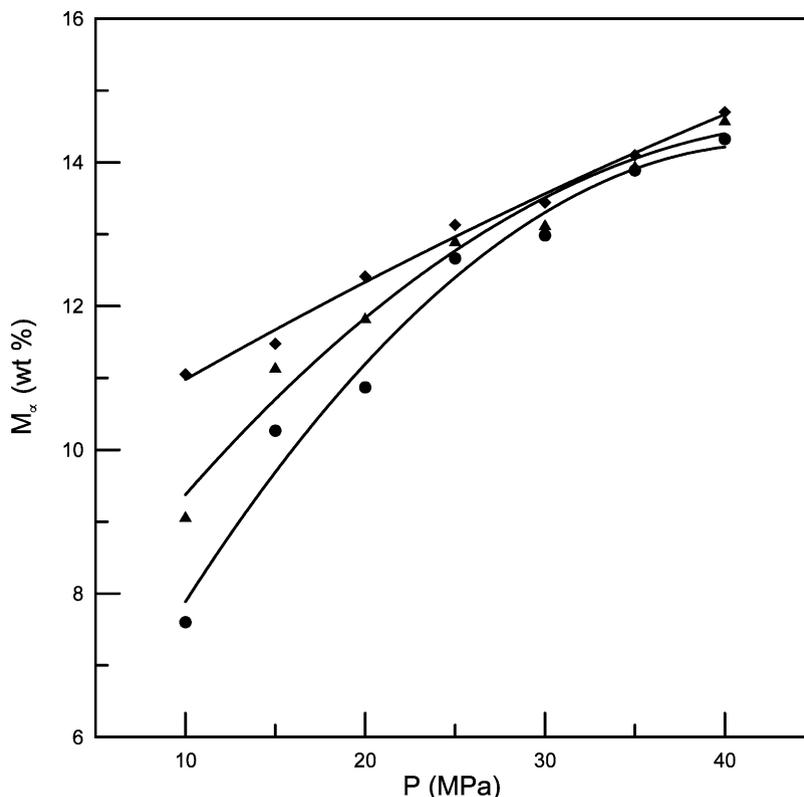


Fig. 5. Plot of the CO₂ equilibrium sorption amount (M_{∞}) against the pressure at various temperatures: ◆, 40 °C; ▲, 50 °C; ●, 60 °C.

up to the second layer of a polymer site. This model is used to explain the solubility of gas in a glassy state polymer. At a higher temperature, the kinetic motion of SCCO₂ increases, and hence results in a decrease in sorption amount. At a higher density region, more SCCO₂ has been absorbed into the polymer. The sorption amount increases with temperature owing to the increase in polymer chain mobility to accommodate more CO₂ molecules [10]. The M_{∞} data from this study at 50 °C under various densities of SCCO₂ are also compared with literature values [10], as shown in Fig. 6.

3.2. Desorption kinetics and diffusivities

The desorption diffusivity D_d of CO₂ from PC specimen at ambient temperature and pressure was evaluated by the negative slope from plot of (M_d/M_{∞}) against $(\sqrt{t_d}/\ell)$ at small desorption time. An example based on the experimental sorption at 40 °C and 30

MPa is shown in Fig. 7. Similar method is employed to determine the D_d values based on other sorption conditions and a plot of D_d against M_{∞} is presented in Fig. 8. The maximum value of D_d is 2.55×10^{-11} m²/s with the highest M_{∞} obtained at 40 °C and 40 MPa. The minimum D_d is 4.6×10^{-12} m²/s with the lowest M_{∞} at 60 °C and 10 MPa. These data are in the similar range with those obtained by Muth et al. [18] for the desorption of CO₂ from PVC. It is indicated in Fig. 8 that D_d increases with the CO₂ concentration inside the PC specimen. Similar effect has also been presented in literature [16,18] for other polymers.

3.3. Sorption kinetics and sorption diffusivities

The sorption diffusivities D_s are determined from the sorption curves shown in Fig. 4. The sorption amount data $\ln(1 - M_s/M_{\infty})$ are plotted against (t_s/ℓ^2) and an example is shown in Fig. 9 based on the experiment data at 40 °C and 30 MPa. According to Eq. (3),

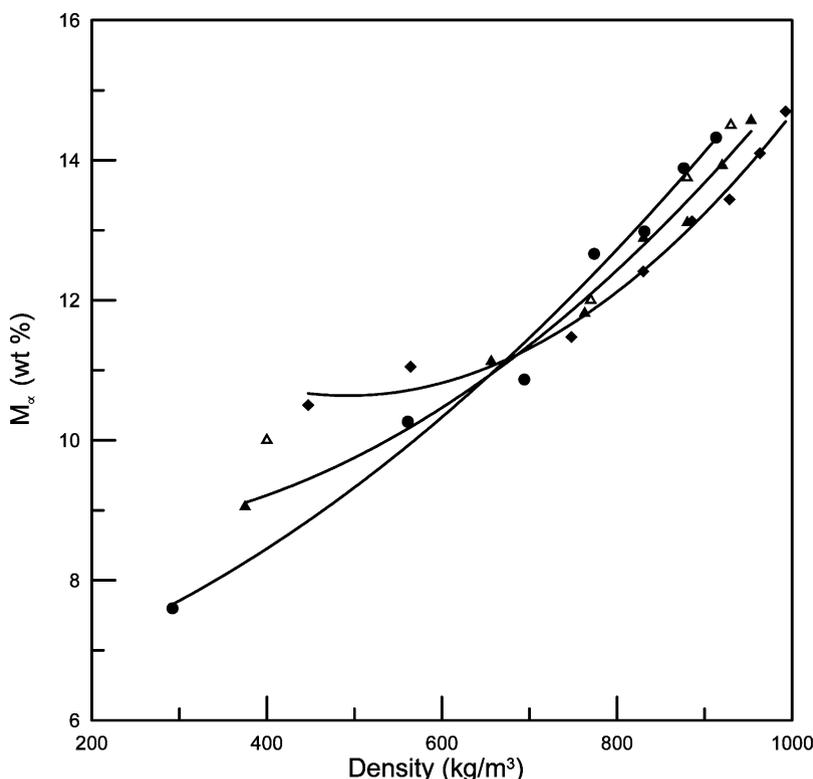


Fig. 6. Plot of the CO₂ equilibrium sorption amount (M_{∞}) against SCCO₂ density at various temperatures: \blacklozenge , 40 °C; \blacktriangle , 50 °C; \bullet , 60 °C (\triangle : literature data at 50 °C [10]).

the slope of the linear plot yields D_s . The calculated D_s values at various temperatures and pressures are presented in Fig. 10. At each fixed pressure, D_s increases with increasing temperature and reaches a maximum value of $3.4 \times 10^{-11} \text{ m}^2/\text{s}$ at 60 °C and 20 MPa. It is believed that the driving force of mass transfer increases and the resistance decreases due to higher polymer chain mobility at higher temperature. At a lower temperature like 40 °C, D_s is smaller at a higher pressure. The SCCO₂ would be more liquid-like at a lower temperature and a higher pressure, and hence leads to a lower diffusivity. Catchpole et al. [20] presented the similar viewpoint as they suggested an equation in estimating the diffusion coefficient for near critical fluids. They proposed that within the reduced density range of $1 < \rho_r < 2.5$, the diffusivity is related with SCCO₂ density by $(-2/3)$ power. The decreasing of diffusivity by increasing density or pressure may also be due to the increasing viscosity

in SCCO₂ phase. The crossover phenomenon of D_s at 40 MPa is observed in Fig. 10. This observation suggests a significant physical change in the polymer phase. It is known that glass transition temperature T_g of a polymer will be lowered at a higher pressure [10]. Schnitzler and Eggers [10] have presented that T_g of PC decreases to 70 °C under SCCO₂ at 30 MPa. In our sorption experiment at 40 MPa, the T_g of PC could be lower than 60 °C. The polymer changed from its glassy state to rubbery state as temperature increased from 40 to 60 °C at 40 MPa. The mobility of the polymer chain was enhanced during this transition, and this resulted in a significant increase in diffusivity as shown in Fig. 10. Visible changes of PC specimen were observed at 60 °C and 40 MPa as shown in Fig. 11. The specimen was initially transparent, as shown in Fig. 11(a). It became opaque after the sorption process, which had not been found at other temperatures and pressures.

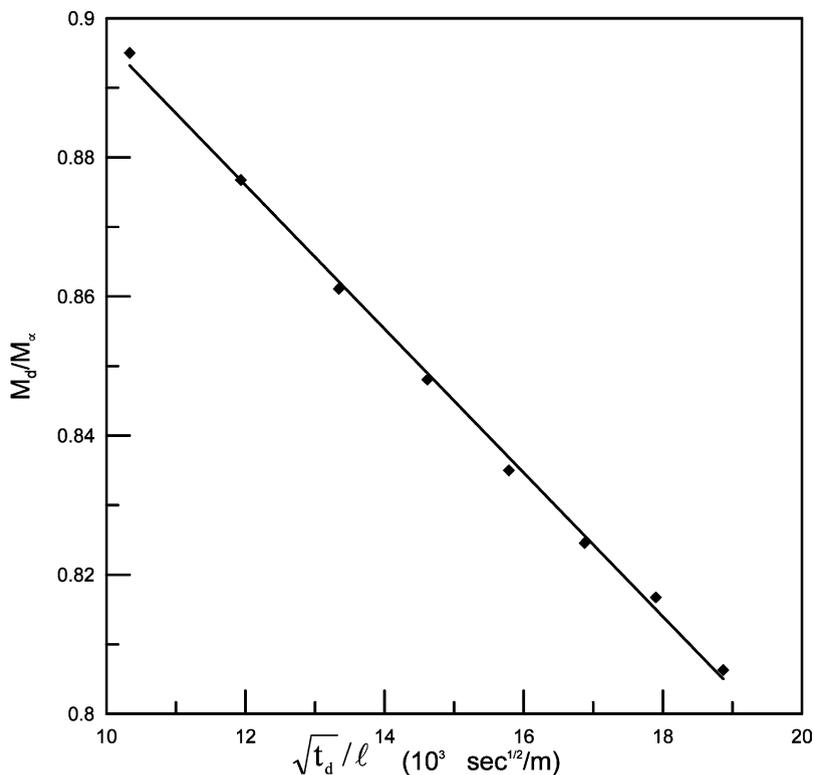


Fig. 7. Plot of M_d/M_∞ against $\sqrt{t_d}/l$ of 4 h sorbed specimen at 40 °C and 30 MPa.

3.4. Plasticizing effect on polymer

The experimental data of the density of SCCO₂, M_∞ , D_d and D_s in this study are summarized in Table 1. Numerical value of D_d is usually larger than that of D_s at 40 and 50 °C, while the tendency is reversed at 60 °C. Muth et al. [18] investigated the

SCCO₂ diffusion into PVC and they reported that the D_d is 3–25 times smaller than D_s . They explained that the sorption process of carbon dioxide was under supercritical condition but the desorption proceeded at ambient temperature and pressure. The higher temperature and pressure of SCCO₂ in the sorption process attributed a larger diffusivity. In this study, we explain

Table 1

Comparison of equilibrium sorption amount, desorption diffusivity and sorption diffusivity at various temperatures and pressures

T (°C)	P (MPa)	Density of SCCO ₂ ^a (kg/m ³)	M_∞ (wt.%)	D_d (10^{-11} m ² /s)	D_s (10^{-11} m ² /s)
40	20	830.04	12.41	2.01	1.22
40	30	928.42	13.44	2.16	1.07
40	40	992.50	14.70	2.55	0.91
50	20	763.12	11.71	1.61	1.68
50	30	880.24	13.13	1.85	1.19
50	40	953.02	14.59	2.07	1.63
60	20	694.03	10.87	1.67	3.36
60	30	831.24	12.98	1.70	1.59
60	40	913.09	14.32	2.07	2.74

^a Evaluated using the Peng–Robinson equation of state.

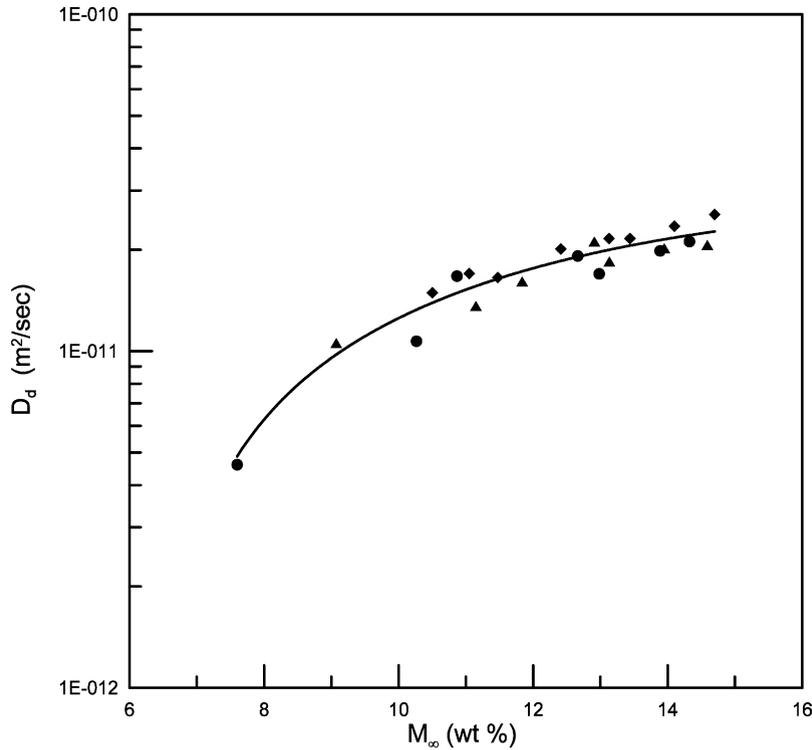


Fig. 8. Plot of the CO₂ desorption diffusivity (D_d) against the equilibrium sorption amount at various sorption temperatures: ◆, 40 °C; ▲, 50 °C; ●, 60 °C.

the difference between D_d and D_s for the diffusion of SCCO₂ in PC by the different states of the polymer phase during sorption and desorption. During the sorption process, the polymer substrate was rigid. The infusion of carbon dioxide has to overcome larger resistance due to lower chain mobility of neat polymer substrate. During the desorption process, however, the polymer substrate has been swollen and plasticized, the exudation of carbon dioxide suffered less resistance due to higher chain mobility of the polymer substrate. Previous authors [6,7] have proposed the acceleration of penetrant diffusion in CO₂ plasticized polymer substrate. About one to four orders of magnitude increase of diffusivity for gas penetrant upon plasticizing has been suggested [6]. In this study, the penetrated CO₂ diffused in the self-plasticized polymer substrate during the desorption process and demonstrated larger D_d than D_s values at 40 and 50 °C. At higher temperature and pressure, larger D_s values are observed due to the change of polymer states.

The plasticizing effect has been verified by tensile testing in this study. The tested specimens have been ground into “I” shape by grinding wheel as shown in Fig. 12(a). Testing has been conducted with 50 mm/min pulling speed and 20 kg maximum loading. The CO₂-swollen PC polymer substrates were prepared by soaking the “I” shape specimen into high pressure vessel under 40 °C and 40 MPa for 4 h. After venting, neither visible deformation nor opaque phenomena were observed as shown in Fig. 12(c). The tensile stresses were measured at 160 s after venting. The first 100 s were spent for transferring the sample from the experimental equipment to the tensile machine location. The other 60 s were used to unload and bind the sample onto the tensile meter. After binding the sample, the tensile test was accomplished within 10 s. The CO₂ amount remained in the sample after the test was measured about 11.3 wt.%, while an initial saturated state had a concentration of 14.7 wt.%. Each of specimens was tested twice to verify

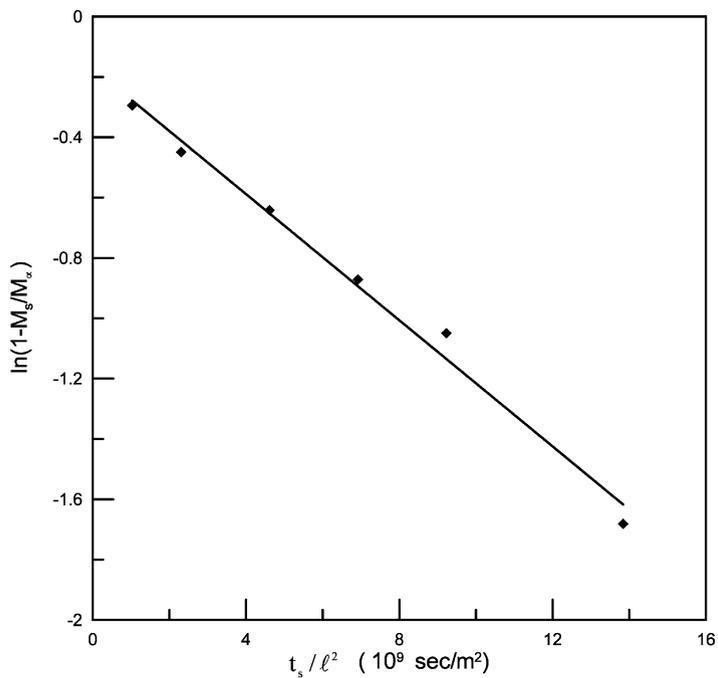


Fig. 9. Plot of $\ln(1-M_s/M_\infty)$ against t_s/ℓ^2 based on the experimental data at 40°C and 30 MPa.

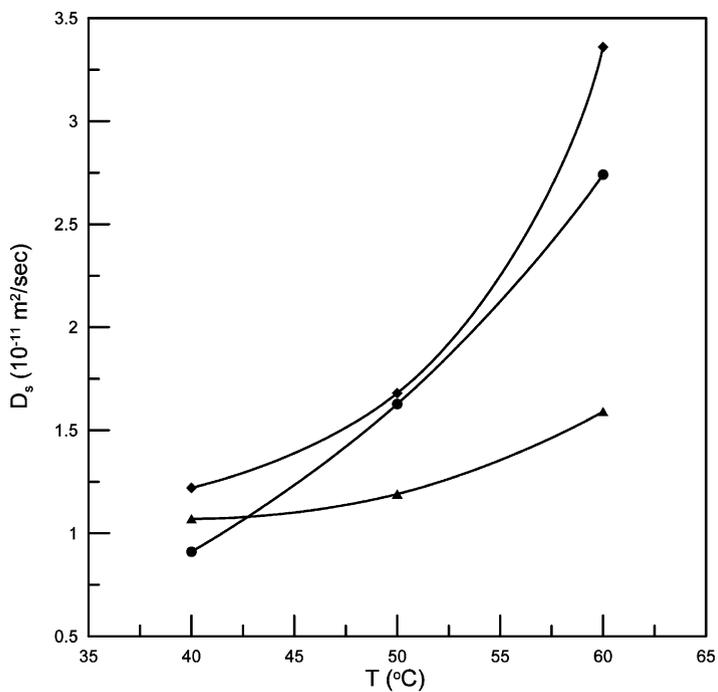


Fig. 10. Variation of sorption diffusivity (D_s) against SCCO₂ temperatures at various pressures: \blacklozenge , 20 MPa; \blacktriangle , 30 MPa; \bullet , 40 MPa.

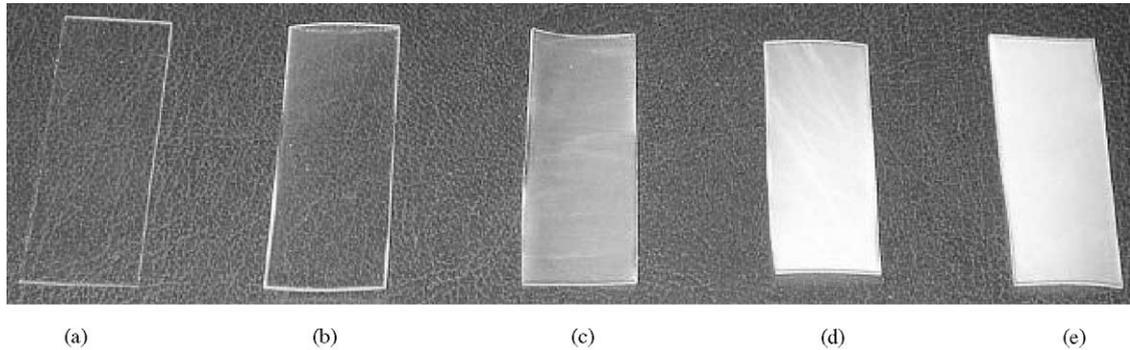


Fig. 11. Photographs of specimens after sorption at 60 °C and 40 MPa SCCO₂ at various sorption times: (a) zero, (b) 40 min, (c) 60 min, (d) 120 min, (e) 240 min.

the reproducibility. The results of tensile testing are shown in Fig. 12. As shown in Fig. 12(b and d), the elongation of CO₂-swollen specimen is much longer than that of the neat PC specimen. It is due to the increase of PC polymer chain mobility by plasticizing of the small CO₂ molecules. The yielding stress of the CO₂-swollen specimen is 32.4 MPa. This is about half

with respect to the yielding stress of 68.1 MPa for the neat PC specimen. The plasticizing effect of increasing chain mobility is known to accelerate the diffusion of CO₂ in polymer substrate [6]. We conclude that there are two factors, the state of penetrant CO₂ and the state of polymer substrate, have to be considered during the diffusion process. At higher temperature

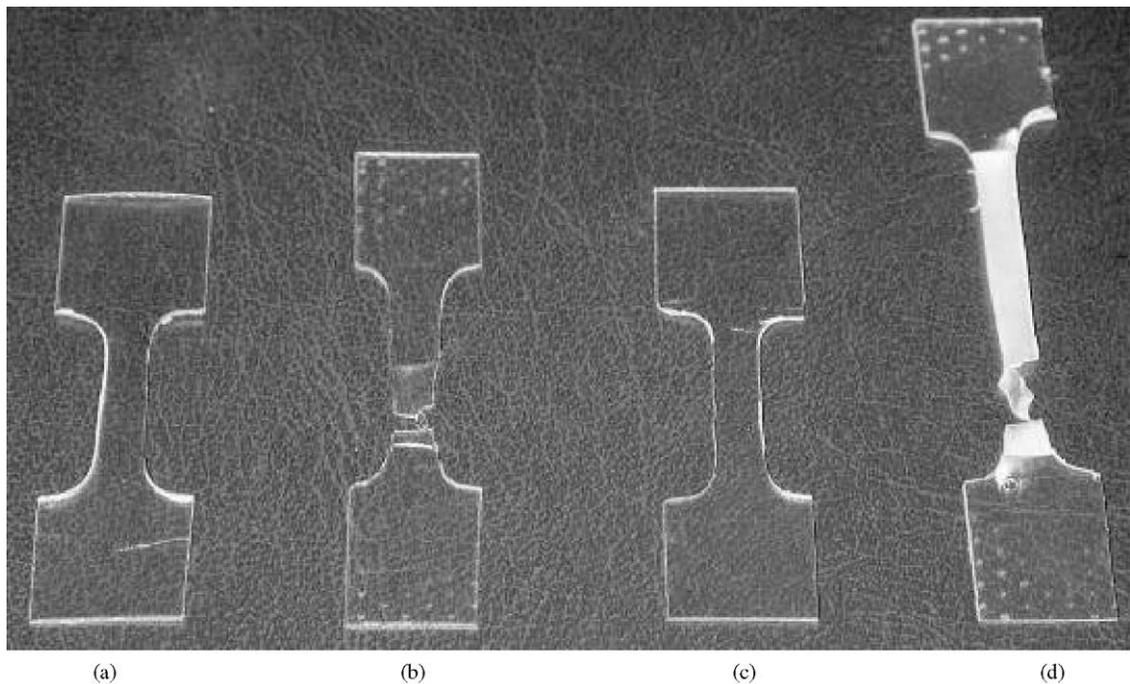


Fig. 12. Photographs of specimens used in tensile testing (a) neat PC, (b) neat PC after testing, (c) CO₂-swollen PC, (d) CO₂-swollen PC after testing under sorption at 40 °C, 40 MPa for 4 h.

and pressure, these competing factors lead to $D_s > D_d$. On the other conditions, the CO₂ plasticizing effect on polymer phase attributes to $D_d > D_s$.

4. Conclusions

In this study, sorption and diffusion of CO₂ into PC specimen at temperatures ranged from 40 to 60 °C and pressures ranged from 10 to 40 MPa are presented. The CO₂ sorption amount into PC increases with pressure and reach a highest value of 14.7 wt.% at 40 °C and 40 MPa. The crossover of sorption isotherm against SCCO₂ density was observed and the change of mass transfer mechanism is suggested. The desorption diffusivity isotherms increase with CO₂ concentration in the PC specimen and reach a higher value of 2.55×10^{-11} m²/s at 40 °C and 40 MPa. The sorption diffusivities increase with temperature and reach a higher value of 3.36×10^{-11} m²/s at highest temperature and lowest pressure. The opaque PC specimen was observed at 60 °C and 40 MPa. The glass transition state was reached and this leads to a large increase of the sorption diffusivities. It is suggested that plasticizing effect of CO₂ on PC is the dominating factor for $D_d > D_s$ in this study. The plasticizing effect on PC specimen has also been verified by tensile testing.

Acknowledgements

The authors are grateful to the National Science Council, ROC for supporting this study.

References

- [1] J.L. Kendall, D.A. Canelas, J.L. Young, J.M. DeSimone, Polymerizations in supercritical carbon dioxide, *Chem. Rev.* 99 (1999) 543.
- [2] S.L. Shenoy, I. Kaya, C. Erkey, R.A. Weiss, Synthesis of conductive elastomeric foams by an in situ polymerization of pyrrole using supercritical carbon dioxide and ethanol cosolvents, *Synth. Met.* 123 (2001) 509.
- [3] M. Tang, T.Y. Wen, T.B. Du, Y.P. Chen, Synthesis of electrically conductive polypyrrole-polystyrene composites using supercritical carbon dioxide: I. Effects of the blending conditions, *Eur. Polym. J.* 39 (2003) 143–149.
- [4] M. Tang, T.Y. Wen, T.B. Du, Y.P. Chen, Synthesis of electrically conductive polypyrrole-polystyrene composites using supercritical carbon dioxide: II. Effects of the doping conditions, *Eur. Polym. J.* 39 (2003) 151–156.
- [5] T.B. Du, M. Tang, Y.P. Chen, Synthesis of the conductive polymer composite using supercritical carbon dioxide, presented at the 8th Meeting on Supercritical Fluids Bordeaux, France, April 14–17, 2002.
- [6] A.R. Berens, G.S. Huvard, R.W. Korsmeyer, F.W. Kunig, Application of compressed carbon dioxide in the incorporation of additives into polymers, *J. Appl. Polym. Sci.* 46 (1992) 231.
- [7] A. Bos, I.G.M. Pünt, M. Wessling, H. Strathmann, CO₂-induced plasticization phenomena in glassy polymers, *J. Membr. Sci.* 155 (1999) 67.
- [8] D. Li, B. Han, Impregnation of polyethylene (PE) with styrene using supercritical CO₂ as the swelling agent and preparation of PE/polystyrene composites, *Ind. Eng. Chem. Res.* 39 (2000) 4506.
- [9] O. Muth, T. Hirth, H. Vogel, Polymer modification by supercritical impregnation, *J. Supercrit. Fluids* 17 (2000) 65.
- [10] J. von Schnitzler, R. Eggers, Mass transfer in polymers in a supercritical CO₂—atmosphere, *J. Supercrit. Fluids* 16 (1999) 81.
- [11] Y. Zhang, K.K. Gangwani, R.M. Lemert, Sorption and swelling of copolymers in the presence of supercritical fluid carbon dioxide, *J. Supercrit. Fluids* 11 (1997) 115.
- [12] J.H. Aubert, Solubility of carbon dioxide in polymers by the quartz crystal microbalance technique, *J. Supercrit. Fluids* 11 (1998) 163.
- [13] Y. Sato, K. Fujiwara, T. Takikawa, S. Sumarno, Takishima, H. Masuoka, Solubilities of carbon dioxide and nitrogen in polystyrene under high temperature and pressure, *Fluid Phase Equilib.* 125 (1996) 129.
- [14] Y. Sato, K. Fujiwara, T. Takikawa, S. Sumarno, Takishima, H. Masuoka, Solubilities and diffusion coefficients of carbon dioxide and nitrogen in polystyrene, high—density polyethylene, and polystyrene under high pressures and temperature, *Fluid Phase Equilib.* 162 (1999) 261.
- [15] Y. Sato, T. Takikawa, S. Takishima, H. Masuoka, Solubilities and diffusion coefficients of carbon dioxide in poly (vinyl acetate) and polystyrene, *J. Supercrit. Fluids* 19 (2001) 187.
- [16] A.R. Berens, G.S. Huvard, Interaction of polymers with near-critical carbon dioxide, K.P. Johnston, J.M.L. Penninger (Eds.), *Supercritical Fluid Science and Technology*, ACS Symposium Series 406, 1989, American Chemical Society, Washington, DC, Chapter 14.
- [17] K.F. Webb, A.S. Teja, Solubility and diffusion of carbon dioxide in polymers, *Fluid Phase Equilib.* 158–160 (1999) 1029.
- [18] O. Muth, T. Hirth, H. Vogel, Investigation of sorption and diffusion of supercritical carbon dioxide into poly (vinyl chloride), *J. Supercrit. Fluids* 19 (2001) 299.
- [19] J. Crank, *Mathematics of Diffusion*, second ed, Oxford University Press, Elsevier, Oxford, 1975.
- [20] O.J. Catchpole, M.B. King, Measurement and correlation of binary diffusion coefficients in near critical fluids, *Ind. Eng. Chem. Res.* 33 (1994) 1828.