

行政院國家科學委員會專題研究計畫 成果報告

高階布氏方程式之非線性特性分析

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高階布氏方程式之非線性特性分析

The Study of Nonlinear Properties of high-order Boussinesq equations

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一、中文摘要

關鍵詞：布氏方程式，二階史托克交互作用，非線性參數

欲瞭解高階布氏方程式的非線性效應，吾人首先將推導四階之布氏方程式。並由二階史托克交互作用分析其超諧和及次諧和轉換係數，選擇適當的水深參數，吾人可獲得最佳化之布氏方程式。

二、英文摘要

Keywords: *Boussinesq equations, second-order Stokes-type Interaction, nonlinear parameters*

The nonlinear characteristics of the $\alpha(\sim^4)$ Boussinesq equations are investigated herein. After deriving the set of high-order Boussinesq equations, the super- and subharmonic transfer coefficients of the wave interaction are analyzed. These coefficients represent the behaviors of the second-order Stokes-type interaction. By comparing the present coefficients to the exact solution, the optimal model can be determined by choosing a suitable water-depth parameter.

三、研究方法及內容

3.1 控制方程式與邊界條件

首先將無因次控制方程式與邊界條件

表示如下

$$\sim^2 \nabla^2 \Phi + \frac{\partial^2 \Phi}{\partial z^2} = 0 \quad \text{at } -h \leq z \leq \nu y \quad (1)$$

$$\frac{\partial \Phi}{\partial z} = \sim^2 \left(\frac{\partial y}{\partial t} + \nu \nabla \Phi \cdot \nabla y \right) \quad \text{at } z = \nu y \quad (2)$$

$$\frac{\partial \Phi}{\partial z} = -\sim^2 (\nabla \Phi \cdot \nabla h) \quad \text{at } z = -h \quad (3)$$

$$\frac{\partial \Phi}{\partial t} + y + \frac{\nu}{2} \left[(\nabla \Phi)^2 + \frac{1}{\sim^2} \left(\frac{\partial \Phi}{\partial z} \right)^2 \right] = 0 \quad \text{at } z = \nu y \quad (4)$$

此處 $\nu = h_0 a_0^{-1}$ 和 $\sim = k_0 h_0$ 為代表非線性及分散性之兩個參數。對於弱非線性條件而言，必須滿足 $\nu = \sim^2 < 1$ 此關係。將式(1)由 $z = -h$ 積分至 $z = \nu y$ ，並考慮式(2)及式(3)之邊界條件，我們可得

$$\nabla \cdot \int_{-h}^{\nu y} \nabla \Phi dz + \frac{\partial y}{\partial t} = 0 \quad (5)$$

以上即為控制方程式與邊界條件。

3.2 理論解析

令速度勢 Φ 為

$$\Phi(x, y, z, t) = \sum_0^{\infty} \sim^{2n} \Phi_n(x, y, z, t) \quad (6)$$

將式(6)代入式(1)及式(3)，則可得

$$\Phi_0 = \Phi_{00}(x, y, t)$$

$$\Phi_1 = \Phi_{10}(x, y, t) - z \nabla \cdot (h \nabla \Phi_{00})$$

$$- \frac{z^2}{2} \nabla^2 \Phi_{00}$$

$$\begin{aligned}
\Phi_2 = & \Phi_{20}(x, y, t) + z \\
& \left[-\nabla \cdot (\hbar \nabla \Phi_{10}) - \frac{\hbar^2}{2} \nabla^2 \nabla \cdot (\hbar \nabla \Phi_{00}) \right. \\
& \left. \frac{\hbar^3}{6} \nabla^2 \nabla^2 \Phi_{00} - \hbar \nabla \nabla \cdot (\hbar \nabla \Phi_{00}) \cdot \nabla h \right. \\
& \left. + \frac{\hbar^2}{2} \nabla \nabla^2 \Phi_{00} \cdot \nabla h \right] \\
& - \frac{z^2}{2} \nabla^2 \Phi_{10} + \frac{z^3}{6} \nabla^2 \nabla \cdot (\hbar \nabla \Phi_{00}) \\
& + \frac{z^4}{24} \nabla^2 \nabla^2 \Phi_{00} \\
& + \sim^2 \nabla \cdot \left\{ + \frac{\hbar^2}{2} \nabla \nabla \cdot (\hbar \nabla \Phi_m) - \frac{\hbar^3}{6} \nabla \nabla^2 \Phi_m \right\} \\
& + \nu \sim^2 \nabla \cdot \left\{ \mathcal{Y} \left[z_m \nabla \cdot (\hbar \nabla \Phi_m) + \frac{z_m^2}{2} \nabla^2 \Phi_m \right] \right\} \\
& + \sim^4 \nabla \cdot \left\{ - \frac{\hbar^3}{6} \nabla \nabla^2 \left[z_m \nabla \cdot (\hbar \nabla \Phi_m) + \frac{z_m^2}{2} \nabla^2 \Phi_m \right] \right. \\
& \left. \hbar \nabla G_1 + \frac{\hbar^2}{2} \nabla G_2 - \frac{\hbar^4}{24} \nabla \nabla^2 \nabla \cdot (\hbar \nabla \Phi_m) + \frac{\hbar^5}{120} \nabla \nabla^2 \nabla^2 \Phi_m \right\} = 0
\end{aligned} \tag{9}$$

及

令 Φ_m 為任意水深處 $z = z_m(x, y)$ 之勢函數，並令 $z = z_m$ ，可得

$$\begin{aligned}
\Phi_m = & \Phi_{00} + \sim^2 \left[\Phi_{10} - z_m \nabla \cdot (\hbar \nabla \Phi_{00}) - \frac{1}{2} z_m^2 \nabla^2 \Phi_{00} \right] \\
& + \sim^4 \left\{ \Phi_{20} + z_m \left[-\nabla \cdot (\hbar \nabla \Phi_{10}) \right. \right. \\
& \left. - \frac{\hbar^2}{2} \nabla^2 \nabla \cdot (\hbar \nabla \Phi_{00}) + \frac{\hbar^3}{6} \nabla^2 \nabla^2 \Phi_{00} \right. \\
& \left. - \hbar \nabla \nabla \cdot (\hbar \nabla \Phi_{00}) \cdot \nabla h + \frac{\hbar^2}{2} \nabla \nabla^2 \Phi_{00} \cdot \nabla h \right] \\
& \left. - \frac{z_m^2}{2} \nabla^2 \Phi_{10} + \frac{z_m^3}{6} \nabla^2 \nabla \cdot (\hbar \nabla \Phi_{00}) \right. \\
& \left. + \frac{z_m^4}{24} \nabla^2 \nabla^2 \Phi_{00} \right\} + \mathcal{O}(\sim^6)
\end{aligned} \tag{7}$$

故

$$\begin{aligned}
\Phi_{00} = & \Phi_m + \sim^2 \left[z_m \nabla \cdot (\hbar \nabla \Phi_m) + \frac{z_m^2}{2} \nabla^2 \Phi_m \right] \\
& + \mathcal{O}(\sim^4) \\
\Phi_{10} = & \mathcal{O}(\sim^2) \\
\Phi_{20} = & \mathcal{O}(\sim^4)
\end{aligned} \left. \right\} \text{改寫為} \tag{8}$$

因此長波方程式可表為

$$\begin{aligned}
& \frac{\partial \mathcal{Y}}{\partial t} + \nabla \cdot [(h + \nu \mathcal{Y}) \nabla \Phi_m] \\
& + \sim^2 \nabla \cdot \left\{ \hbar \nabla \left[z_m \nabla \cdot (\hbar \nabla \Phi_m) + \frac{z_m^2}{2} \nabla^2 \Phi_m \right] \right\}
\end{aligned}$$

$$\begin{aligned}
& \mathcal{Y} + \frac{\partial \Phi_m}{\partial t} \\
& + \sim^2 \left[z_m \nabla \cdot \left(\hbar \nabla \frac{\partial \Phi_m}{\partial t} \right) + \frac{z_m^2}{2} \nabla^2 \left(\frac{\partial \Phi_m}{\partial t} \right) \right] + \frac{\nu}{2} (\nabla \Phi_m)^2 \\
& + \sim^4 \left\{ z_m G_3 + \frac{z_m^2}{2} \nabla^2 \left[z_m \nabla \cdot \left(\hbar \nabla \frac{\partial \Phi_m}{\partial t} \right) + \frac{z_m^2}{2} \nabla^2 \left(\frac{\partial \Phi_m}{\partial t} \right) \right] \right. \\
& \left. - \frac{z_m^3}{6} \nabla^2 \nabla \cdot \left(\hbar \nabla \frac{\partial \Phi_m}{\partial t} \right) - \frac{z_m^4}{24} \nabla^2 \nabla^2 \left(\frac{\partial \Phi_m}{\partial t} \right) \right\} \\
& + \nu \sim^2 \left\{ \frac{1}{2} [\nabla \cdot (\hbar \Phi_m)]^2 - \mathcal{Y} \nabla \cdot \left(\hbar \nabla \frac{\partial \Phi_m}{\partial t} \right) \right\} = 0
\end{aligned} \tag{10}$$

其中 G_1 、 G_2 及 G_3 為與深度 z 有關的變數。(9)式及(10)式即為以任意水深處之速度勢為變數之長波方程式。現在考慮定水深且流場為二維流場，並令水深參數 $m = \frac{z_m}{h}$ ($-1 \leq m \leq 0$)，則上二式可

$$\begin{aligned}
& \frac{\partial \mathcal{Y}}{\partial t} + \frac{\partial}{\partial x} \left[(h + \nu \mathcal{Y}) \frac{\partial \Phi_m}{\partial x} \right] + \sim^2 \hbar^3 H_1 \frac{\partial^4 \Phi_m}{\partial x^4} \\
& + \sim^4 \hbar^5 H_2 \frac{\partial^6 \Phi_m}{\partial x^6} + \nu \sim^2 \hbar^2 H_3 \frac{\partial}{\partial x} \left[\mathcal{Y} \frac{\partial^3 \Phi_m}{\partial x^3} \right] = 0
\end{aligned} \tag{11}$$

$$\begin{aligned}
& \frac{\partial \Phi_m}{\partial t} + \mathcal{Y} + \sim^2 \hbar^2 H_3 \frac{\partial^3 \Phi_m}{\partial x^2 \partial t} + \frac{\nu}{2} \left(\frac{\partial \Phi_m}{\partial x} \right)^2 \\
& + \sim^4 \hbar^4 H_4 \frac{\partial^5 \Phi_m}{\partial x^4 \partial t} + \nu \sim^2 \left[-\hbar \mathcal{Y} \frac{\partial^3 \Phi_m}{\partial x^2 \partial t} + \frac{\hbar^2}{2} \left(\frac{\partial^2 \Phi_m}{\partial x^2} \right)^2 \right] = 0
\end{aligned}$$

(12)

其中

$$H_1 = \frac{1}{2}m^2 + m + \frac{1}{3} \quad (13.a)$$

$$H_2 = \frac{5}{24}m^4 + \frac{5}{6}m^3 + \frac{7}{6}m^2 + \frac{2}{3}m + \frac{2}{15} \quad (13.b)$$

$$H_3 = \frac{1}{2}m^2 + m \quad (13.c)$$

$$H_4 = \frac{5}{24}m^4 + \frac{5}{6}m^3 + m^2 + \frac{1}{3}m \quad (13.d)$$

(9)、(10)式及(11)、(12)式即為以任意水深之速度勢為變數之弱非線性長波方程式，在此吾人稱其為「新布氏方程式」。

四、布氏方程式之非線性特性探討

為分析布氏方程式之非線性特性，在此吾人引入二階史托克交互作用。首先，吾人令

$$\mathcal{Y} = \mathcal{Y}_0 + \nu \mathcal{Y}_1 + \nu^2 \mathcal{Y}_2 + \dots \quad (12)$$

$$\Phi_m = \Phi_0 + \nu \Phi_1 + \nu^2 \Phi_2 + \dots \quad (13)$$

吾人將 \mathcal{Y} 及 Φ 代入原布氏方程式，並依 ν 的冪次排序，可得

$$\frac{\partial \mathcal{Y}_n}{\partial t} + L_1 \tilde{\Phi}_n = -\nabla \cdot F_n \quad (14)$$

$$\mathcal{Y}_n + L_2 \frac{\partial \tilde{\Phi}_n}{\partial t} = -E_n \quad (15)$$

其中運算子 L_1, L_2 為

$$L_1 = (G_1 \nabla^2 + \sim^2 G_2 \nabla^2 \nabla^2 + \sim^4 G_3 \nabla^2 \nabla^2 \nabla^2)$$

$$L_2 = 1 + \sim^2 H_1 \nabla^2 + \sim^4 H_2 \nabla^2 \nabla^2$$

(14)式及(15)式之右邊項可解得為

$$\begin{cases} F_0 = 0 \\ F_1 = \mathcal{Y}_0 (\nabla + \sim^2 H_1 \nabla \nabla^2 + \sim^4 H_2 \nabla \nabla^2 \nabla^2) \tilde{\Phi}_0 \\ E_0 = 0 \\ E_1 = -L_{2a} \frac{\partial \tilde{\Phi}_0}{\partial t} + \frac{1}{2} (\nabla L_2 \tilde{\Phi}_0)^2 + \\ \sim^2 \left[\frac{G_1^2}{2} (\nabla^2 \tilde{\Phi}_0)^2 \right] + \sim^4 [G_1 G_2 \nabla^2 \tilde{\Phi}_0 \nabla^2 \nabla^2 \tilde{\Phi}_0] \end{cases}$$

令 $\mathcal{Y}_0 = \sum_n a_n \cos_{n,n}$ ， $\tilde{\Phi}_0 = \sum_n b_n \sin_{n,n}$ 代

入(14)及(15)，可得

$$-\nabla \cdot F_1 = \frac{1}{4} \sum_n \sum_l a_n a_l [\mathbf{F}_{nl}^+ \sin(\nu_n + \nu_l) + \mathbf{F}_{nl}^- \sin(\nu_n - \nu_l)] \quad (16)$$

$$\mathbf{F}_{nl}^{\pm} = \frac{\check{S}_n k_n^2 \pm \check{S}_l k_l^2 + (\check{S}_n \pm \check{S}_l)(\bar{k}_n \cdot \bar{k}_l)}{\check{S}_n \check{S}_l} \quad (17)$$

$$-E_1 = \frac{1}{4} \sum_n \sum_l a_n a_l [\mathbf{E}_{nl}^+ \cos(\nu_n + \nu_l) + \mathbf{E}_{nl}^- \cos(\nu_n - \nu_l)] \quad (18)$$

$$\begin{aligned} \mathbf{E}_{nl}^{\pm} = & \frac{1}{\check{S}_n \check{S}_l \hat{H}_n \hat{H}_l} \left[-(\bar{k}_n \cdot \bar{k}_l) \cdot (\hat{H}_n + \hat{H}_l - 1) \right. \\ & \pm k_n^2 k_l^2 (\sim^2 G_1 + \sim^4 G_2 (k_n^2 + k_l^2)) \\ & \left. + k_n^3 k_l^3 (-\sim^4 H_1^2) + \check{S}_n \check{S}_l \hat{H}_n \hat{G}_l + \check{S}_n \check{S}_l \hat{H}_l \hat{G}_n \right] \end{aligned} \quad (19)$$

$$\hat{G}_n = \sim^2 G_1 k_n^2 - \sim^4 G_2 k_n^4 \quad (20)$$

故可得 \mathcal{Y}_1 為

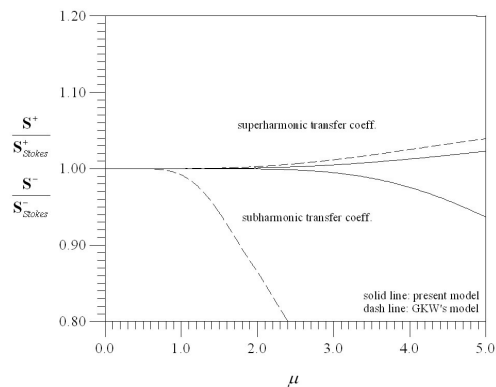
$$\mathcal{Y}_1 = \sum_n \sum_l a_n a_l \{ \mathbf{S}_{nl}^+ \cos(\nu_n + \nu_l) + \mathbf{S}_{nl}^- \cos(\nu_n - \nu_l) \} \quad (21)$$

其中 \mathbf{S}_{nl}^+ 及 \mathbf{S}_{nl}^- 分別稱為超諧和及次諧和轉換係數。

五、結論與討論

為探討上述兩係數的效應，吾人令

$\tilde{S}_n = \tilde{S}_j$, $k_n = k_j$ 。由於選擇不同的水深參數 m 值將會造成不同的結果，我們選定水深範圍為 $0 < \mu < 5$ ，此時的最佳水深參數為 -0.328 。圖一表示超諧和及次諧和轉換係數與正確解之間的關係。和 GKW 於 2000 年的研究成果比較，可發現吾人的成果優於 GKW 的成果，此原因在於 GKW 的最佳化方程式是使用帕德近似所推得，此基本假設並不足以使其非線性效應達到最精確的目標。在爾後的研究中，吾人將試圖將可應用之水深範圍擴大，以加強本模式的適用性。



圖一 超諧和及次諧和轉換係數

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